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POWERGRID
STANDARD RESIN SYSTEMS FOR STRUCTURAL SHAPES

STANDARD POLYESTER (ISO) RESIN SYSTEM

The STANDARD POLYESTER RESIN SYSTEM refers to a NON FLAME RETARDANT isophthalic polyester resin system. This resin system is manufactured in olive green and incorporates ultraviolet inhibitors. Polyester resins exhibit good corrosion resistance, good electrical properties, low thermal conductivity and excellent mechanical properties.

FLAME RETARDANT (ISOFR) RESIN SYSTEM

This resin system exhibits the same characteristics as the Standard Polyester resin system PLUS a flame retardant rating of 25 or less when tested in accordance with ASTM E-84. The FLAME RETARDANT resin system is manufactured in grey and yellow. Other colour options available.

FLAME RETARDANT VINYL ESTER (VEFR) RESIN SYSTEM

This resin system is manufactured from vinyl ester resin which exhibits higher strength, improved strength and stiffness retention at elevated temperatures, and improved corrosion resistance. This system also meets a maximum flame spread rating of 25 and is produced in beige, grey and yellow.

TEMPERATURE EFFECTS

The approximate retention of mechanical properties at elevated temperatures are:

| | TEMPERATURE | ISO/ISOFR | VEFR |
|------------------------------|--------------------|------------------|-------------|
| Ultimate Stress | 100°F | 85% | 90% |
| | 125°F | 70% | 80% |
| | 150°F | 50% | 80% |
| | 175°F | not recommended | 75% |
| | 200°F | not recommended | 50% |
| Modulus of Elasticity | 100°F | 100% | 100% |
| | 125°F | 90% | 95% |
| | 150°F | 85% | 90% |
| | 175°F | not recommended | 88% |
| | 200°F | not recommended | 85% |

The data in this corrosion guide is based on field service performance, laboratory testing and extrapolated values from our resin manufacturers' recommendations. Data shown is intended as a guide only. It is recommended that for a specific application, testing be done in the actual chemical environment.

The following conditions will effect the suitability of a specific resin laminate:

- Periodic changes in temperature
- Temperature spikes
- Changes in chemical concentrations
- Combinations of chemicals
- Exposure to vapors only
- Exposure to frequent splashes and spills
- Exposure to intermittent splashes and spills
- Frequency of maintenance wash down
- Load bearing or non-load bearing requirements

| Chemical Environment | Maximum recommended Service Temperatures °F | | Chemical Environment | Maximum recommended Service Temperatures °F | |
|---------------------------------|---|-----------|--|---|-----------|
| | Vinylester | Polyester | | Vinylester | Polyester |
| Acetic Acid, to 10% | 170 | 80 | Butyl Acetate | NR | NR |
| Acetic Acid, to 50% | 180 | NR | Butyl Alcohol | 80 | NR |
| Acetic Acid, Glacial | NR | NR | Calcium Carbonate | 170 | 120 |
| Acetone | NR | NR | Calcium Hydroxide | 140 | 120 |
| Aluminum Chloride | 170 | 120 | Calcium Hypochlorite | 120 | NR |
| Aluminum Hydroxide | 140 | 120 | Calcium Nitrate | 170 | 120 |
| Aluminum Nitrate | 140 | 120 | Calcium Sulfate | 170 | 120 |
| Aluminum Sulfate | 170 | 120 | Carbon Disulfate | NR | NR |
| Ammonium Chloride | 170 | 120 | Carbon Monoxide Gas | 170 | 160 |
| Ammonium Hydroxide, 5% | 140 | NR | Carbon Dioxide Gas | 170 | 160 |
| Ammonium Nitrate, to 50% | 170 | 120 | Carbon Tetrachloride, Liquid or Vapor | 110 | NR |
| Ammonium Nitrate, Saturated | 170 | NR | Chlorine, Dry Gas | 170 | NR |
| Ammonium Persulfate, to 25% | 140 | 90 | Chlorine, Wet Gas | 170 | NR |
| Ammonium Phosphate | 170 | 120 | Chlorine Water | 140 | NR |
| Ammonium Sulfate | 170 | 120 | Chloroform | NR | NR |
| Amyl Alcohol | 80 | NR | Chromic Acid, to 5% | 110 | NR |
| Barium Carbonate | 170 | 120 | Chromous Sulfate | 140 | 120 |
| Barium Chloride | 170 | 120 | Citric Acid | 170 | 120 |
| Barium Sulfate | 170 | 120 | Copper Chloride | 170 | 170 |
| Benzene | NR | NR | Copper Cyanide | 170 | 170 |
| Benzene Sulfonic Acid 50% | 110 | NR | Copper Nitrate | 170 | 170 |
| Benzoic Acid | 170 | 120 | Crude Oil, Sour | 170 | 170 |
| Benzyl Alcohol | NR | NR | Cyclohexane, Liquid and Vapour | 170 | NR |
| Borax | 170 | 120 | Diesel Fuel | 140 | 90 |
| Brine (Sodium Chloride Sol.) | 170 | 120 | Ethyl Acetate | NR | NR |
| Bromine, Liquid or Vapor | NR | NR | Phosphoric Acid, Vapour | 170 | 120 |
| Ethyl Alcohol | NR | NR | Potassium Aluminum Sulfate | 170 | 120 |
| Ethylene Glycol | 170 | 120 | Potassium Bicarbonate | 110 | 100 |
| Fatty Acids | 170 | 80 | Potassium Carbonate, to 10% | 110 | NR |
| Ferric Chloride | 170 | 10 | Potassium Chloride | 170 | 120 |
| Ferric Sulfate | 170 | 110 | Potassium Hydroxide | 140 | NR |
| Formaldehyde | 110 | NR | Potassium Nitrate | 170 | 120 |
| Fuel Oil | 140 | 80 | Potassium Sulfate | 170 | 120 |
| Gasoline, Aviation and Ethyl | 140 | 80 | Propylene Glycol | 170 | 120 |
| Glucose | 170 | 100 | Sodium Acetone | 170 | 120 |
| Glycerine | 170 | 100 | Sodium Benzoate | 140 | 120 |
| Hexane | 120 | 90 | Sodium Bicarbonate | 140 | 120 |
| Hydraulic Fluid (Glycol Based) | 140 | NR | Sodium Bisulfate | 170 | 120 |
| Hydraulic Fluid Skydraul | 140 | NR | Sodium Bisulfite | 170 | 120 |
| Hydrobromic Acid | 110 | NR | Sodium Borate | 170 | 120 |
| Hydrochloric Acid, up to 15% | 140 | 80 | Sodium Bromide | 170 | 120 |
| Hydrochloric Acid, Concentrated | 110 | NR | Sodium Carbonate, to 10% | 140 | 70 |
| Hydrogen Bromide, Dry Gas | 140 | 80 | Sodium Chloride | 170 | 120 |
| Hydrogen Bromine, Wet Gas | 140 | NR | Sodium Cyanide | 170 | 120 |
| Hydrogen Chloride, Dry Gas | 170 | 80 | Sodium Dichromate | 170 | 120 |
| Hydrogen Chloride, Wet Gas | 170 | 80 | Sodium Diphosphate | 170 | 120 |
| Hydrogen Fluoride, Sol or Vapor | 140 | NR | Sodium Hydroxide, 10% | 140 | NR |
| Hydrogen Peroxide, to 10% | 110 | NR | | | |

| | | | | | |
|--------------------------------|-----|-----|---------------------------------|-----|-----|
| Hydrogen Sulfate, Dry Gas | 140 | 80 | Sodium Hypochlorite, to 5!% | 110 | 70 |
| Hydrogen Sulfate, Wet Gas | 140 | 80 | Sodium Monophosphate | 170 | 120 |
| Isopropyl Alcohol | 80 | NR | Sodium Nitrate | 170 | 120 |
| JP-4 | 140 | 80 | Sodium Nitrite | 170 | 120 |
| Kerosene | 140 | 110 | Sodium Sulfate | 170 | 120 |
| Lactic Acid | 170 | 120 | Sodium Tetraborate | 140 | 120 |
| Lead Acetate | 170 | 120 | Sodium Thiosulfate | 140 | 120 |
| Linseed Oil | 170 | 100 | Soy Oil | 170 | 100 |
| Lithium Chloride | 170 | 120 | Stearic Acid | 170 | 120 |
| Magnesium Carbonate | 170 | 120 | Styrene | NR | NR |
| Magnesium Chloride | 170 | 120 | Sulfamic Acid | 170 | 120 |
| Magnesium Hydroxide | 170 | 100 | Sulfated Detergents | NR | 120 |
| Magnesium Nitrate | 170 | 120 | Sulfite Liquor | 160 | 100 |
| Magnesium Sulfate | 170 | 120 | Sulfur Dioxide, gas-dry | 170 | 120 |
| Mercuric Chloride | 170 | 120 | Sulfur Dioxide, gas-wet | 170 | 70 |
| Mercury Metal | 170 | 120 | Sulfur Trioxide, gas-wet or dry | 170 | NR |
| Methyl Ethyl Ketone | NR | NR | Sulfuric Acid, to 25% | 170 | 80 |
| Mineral Oil | 170 | 120 | Tartaric Acid | 170 | 120 |
| Monochlorobenzene | NR | NR | Tetrachloroethylene | NR | NR |
| Naphtha | 140 | 120 | Toluene | NR | NR |
| Nickel Chloride | 170 | 120 | Trichloroethylene vapour | NR | NR |
| Nitric Acid, to 5% | 110 | 100 | Trisodium Phosphate | 170 | NR |
| Nitric Acid, Concentrated | NR | NR | Urea, 35% | 110 | NR |
| Nitric Acid, Vapour | 140 | 100 | Vinegar | 170 | 150 |
| Oleic Acid | 170 | 120 | Water, Distilled | 180 | 150 |
| Oxalic Acid | 170 | 120 | Water, Tap | 180 | 120 |
| Paper Mill Liquor | 100 | 100 | Zinc Chloride | 170 | 120 |
| Phenol Solution or Vapour | NR | NR | Zinc Nitrate | 170 | 120 |
| Phosphoric Acid | 170 | 100 | Zinc Sulfate | 170 | 120 |
| Phosphoric Acid, Salts thereof | 170 | 120 | | | |

Typical Coupon Properties

The values listed below are test results from coupon tests performed in accordance with the designated ASTM Test.

LW= Lengthwise

CW=Crosswise

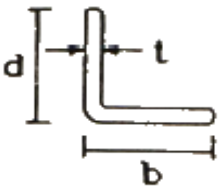
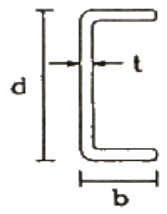
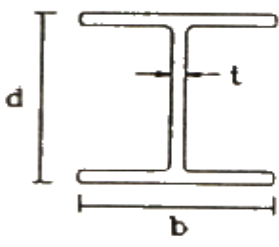
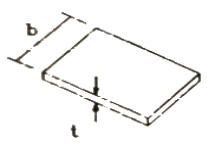
PF= Perpendicular to Laminate Face

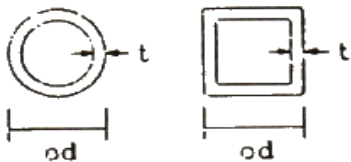
| <u>MECHANICAL PROPERTIES</u> | <u>ASTM</u> | <u>UNITS</u> | <u>VALUE</u> |
|--------------------------------------|--------------|---------------------------|--------------|
| Tensile Stress, LW | D-638 | psi | 30,000 |
| Tensile Stress, CW | D-638 | psi | 7,000 |
| Tensile Modulus, LW | D-638 | 10 ⁶ psi | 2.5 |
| Tensile Modulus, CW | D-638 | 10 ⁶ psi | 0.8 |
| Compressive Stress, LW | D-695 | psi | 30,000 |
| Compressive Stress, CW | D-695 | psi | 15,000 |
| Compressive Modulus, LW | D-695 | 10 ⁶ psi | 2.5 |
| Compressive Modulus, CW | D-695 | 10 ⁶ psi | 1 |
| Flexural Stress, LW | D-790 | psi | 30,000 |
| Flexural Stress, CW | D-790 | psi | 10,000 |
| Flexural Modulus, LW | D-790 | 10 ⁶ psi | 1.8 |
| Flexural Modulus, CW | D-790 | 10 ⁶ psi | 0.8 |
| Modulus of Elasticity, E | Full Section | 10 ⁶ psi | 2.8 |
| Shear Modulus | ----- | 10 ⁶ psi | 0.45 |
| Short Beam Shear | D-2344 | psi | 4,500 |
| Punch Shear | D-732 | psi | 10,000 |
| Bearing Stress, LW | D-953 | psi | 30,000 |
| Notched Izod Impact, LW | D-256 | ft-Lbs/in | 25 |
| Notched Izod Impact, CW | D-256 | ft-Lbs/in | 4 |
| | | | |
| <u>PHYSICAL PROPERTIES</u> | <u>ASTM</u> | <u>UNITS</u> | <u>VALUE</u> |
| Barcol Hardness | D-495 | ----- | 45 |
| 24 Hour Water Absorption | D-570 | % max | 0.45 |
| Density | D-792 | lbs/in ³ | .062 - .070 |
| Coefficient of Thermal Expansion, LW | D-696 | 10 ⁻⁶ in/in/°C | 8 |
| | | | |
| <u>ELECTRICAL PROPERTIES</u> | <u>ASTM</u> | <u>UNITS</u> | <u>VALUE</u> |
| Arc Resistance, LW | D-495 | seconds | 120 |
| Dielectric Strength, LW | D-149 | kv/in | 35 |
| Dielectric Strength, PF | D-149 | volts/mil | 200 |
| Dielectric Constant, PF | D-150 | at 60hz | 5 |

Polyester and Vinylester Fire Retardant Structural Profiles:

| <u>FLAMMABILITY PROPERTIES</u> | <u>ASTM</u> | <u>UNITS</u> | <u>VALUE</u> |
|--------------------------------|-------------|--------------|--------------|
| Tunnel Test | E-84 | Flame Spread | 25 max |
| Flammability | D-635 | ----- | Nonburning |

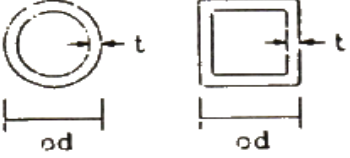
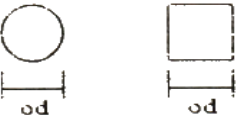
Cross Sectional Tolerances

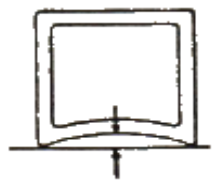
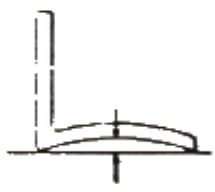
| SHAPE | DIMENSION | TOLERANCES | MAXIMUM OR MINIMUM TOLERANCES |
|--|-----------------|------------|-------------------------------|
| <p align="center">ANGLES</p>  | t = thickness | ± 10% | ± 0.010" minimum |
| | b= flange width | ± 5% | ± 0.094" maximum |
| | d= depth | ± 5% | ± 0.094" maximum |
| <p align="center">CHANNELS</p>  | t = thickness | ± 10% | ± 0.010" minimum |
| | b= flange width | ± 5% | ± 0.094" maximum |
| | d= depth | ± 5% | ± 0.094" maximum |
| <p align="center">BEAMS</p>  | t = thickness | ± 10% | ± 0.010" minimum |
| | b= flange width | ± 5% | ± 0.094" maximum |
| | d= depth | ± 5% | ± 0.094" maximum |
| <p align="center">FLAT SHEET</p>  | t = thickness | ± 10% | ± 0.040" maximum |
| | b= width | ± 3% | ± 0.094" maximum |





Cross Sectional Tolerances

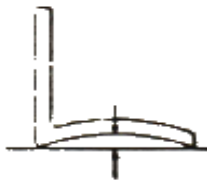
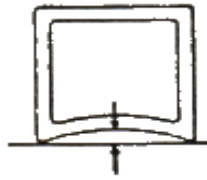
| SHAPE | DIMENSION | OUTSIDE DIMENSION CONDITION | TOLERANCES |
|---|-----------------------|-----------------------------|------------|
| ROUND & SQUARE TUBE  | t = thickness | Under 1" | ± 20% |
| | | 1" and up | ± 15% |
| | od= outside dimension | Under 2" | ± 0.020" |
| | | 2" and up | ± 0.040" |
| ROUND ROD & SQUARE BAR  | od= outside dimension | up to 3" | ± 0.010" |

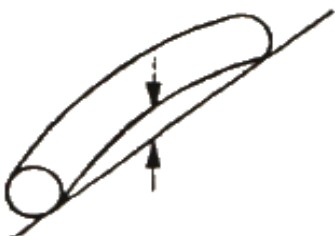
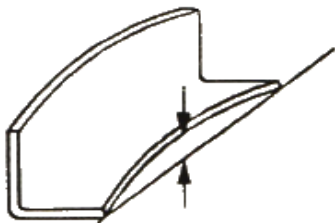




Flatness

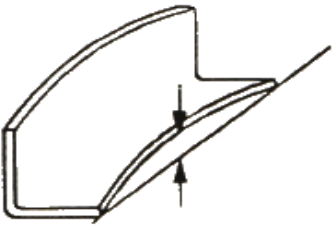
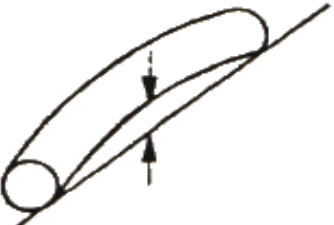

Flatness is measured in the centre with the weight of the profile minimizing the deviation by contact with a flat surface.

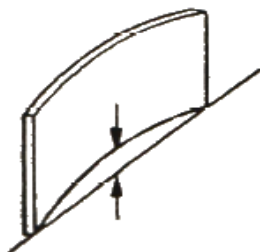
| | | | |
|---|-------------------------------|---------------------------------|------------------------------|
| <p>STRUCTURAL SHAPES, RODS, BARS, & SHEET</p>  | Allowable deviation from flat | | |
| | Width | All Thicknesses | |
| | Up to 1" | 0.008" | |
| | Over 1" | 0.008"/inch | |
| <p>HOLLOW SHAPES</p>  | Allowable deviation from flat | | |
| | Width | Thicknesses 0.125" tp 0.188" | Thickness 0.189" and over |
| | Up to 1" | 0.012" | 0.008" |
| | Over 1" | 0.012"/inch | 0.008"/inch |



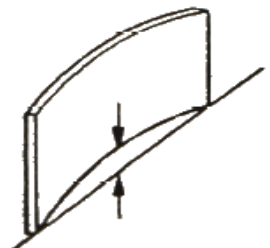
Straightness

Straightness is measured in the centre with the weight of the pultrusion minimizing the deviation by contact with a flat surface.

| | | |
|---|-----------------------------------|-------------|
| <p align="center">ANGLE, BEAM AND CHANNEL</p>  | Allowable deviation from straight | |
| <p align="center">RODS AND BARS</p>  | All widths | 0.050"/foot |
| <p align="center">ROUND, SQUARE, AND RECTANGULAR TUBE</p>  | Allowable deviation from straight | |
| | Diameter/Depth | Per Foot |
| | Up to 1" | 0.020" |
| | Over 1" | 0.040" |

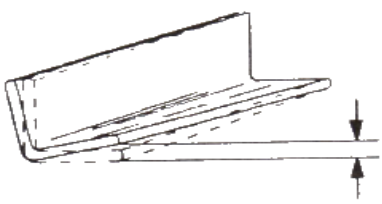




| | | |
|--|-----------------------------------|-------------|
| <p>SHEET AND PLATE</p>  | Allowable deviation from straight | |
| | All thicknesses and widths | 0.025"/foot |

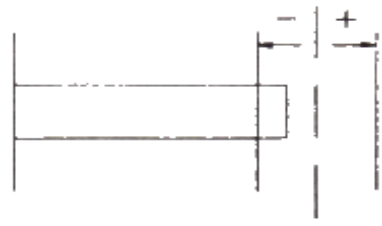
Twist

Twist is measured with the weight of the pultrusion minimizing the twist

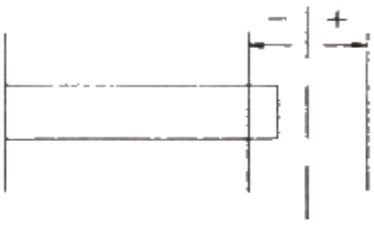
| | | | |
|--|------------------|--------------------------------------|------------------------------------|
| <p>ALL PROFILES</p>  | Allowable twist | | |
| | Width/Depth | Per Foot | Per Piece Max |
| | Up to 1.499" | $\tan 1^\circ \times \text{width}$ | $\tan 7^\circ \times \text{width}$ |
| | 1.500" to 2.999" | $\tan 1/2^\circ \times \text{width}$ | $\tan 5^\circ \times \text{width}$ |
| | 3.000" and over | $\tan 1/3^\circ \times \text{width}$ | $\tan 3^\circ \times \text{width}$ |

Angularity

| | | |
|--------------|---|--|
| ALL PROFILES | Allowable deviation from specific angle | |
| | thickness up to 3/4" | $\tan 1 1/2^\circ \times \text{width of flange in inches}$ |



Cut Lengths

| | | |
|--|---|-----|
| <p align="center">ALL PROFILES</p>  | Allowable deviation from specific angle | |
| | N/A | N/A |
| | | |

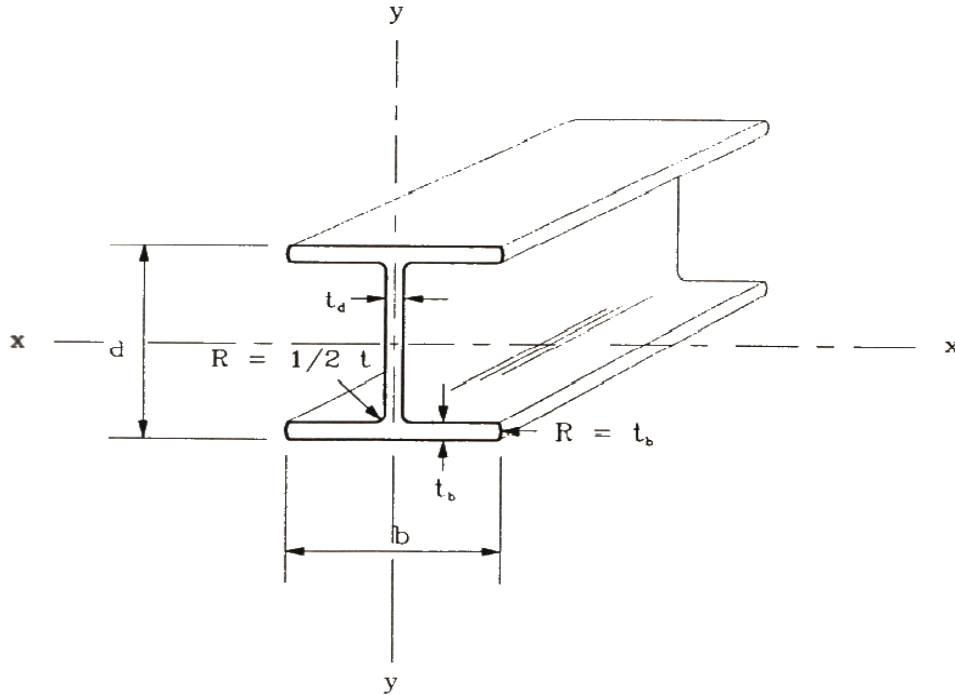
Squareness of Endcut

| | | |
|------------------------------------|---------------------------------|--------------------------|
| <p align="center">ALL PROFILES</p> | Allowable deviation from square | |
| | All thicknesses | tan 1° x width in inches |

Section Properties

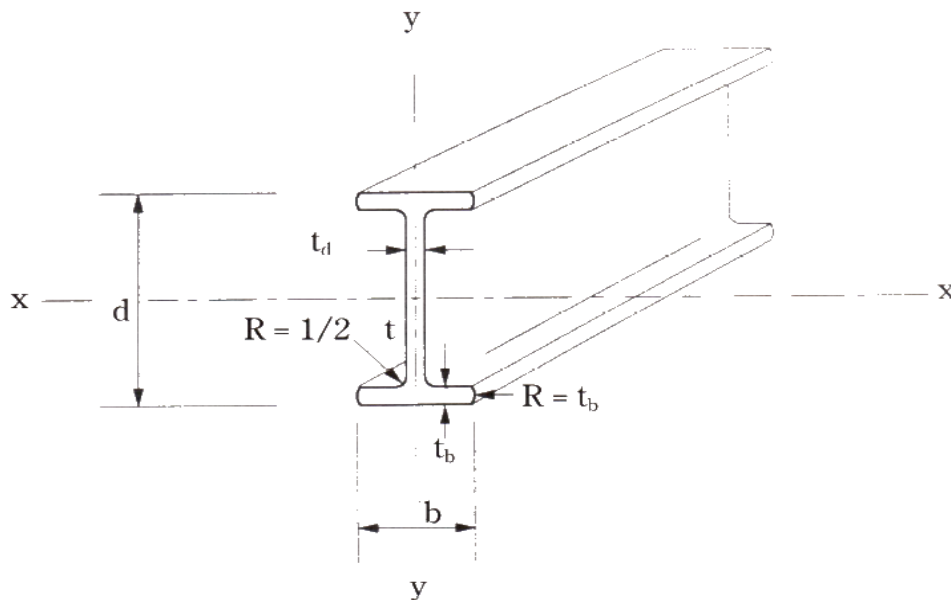
WF-BEAM

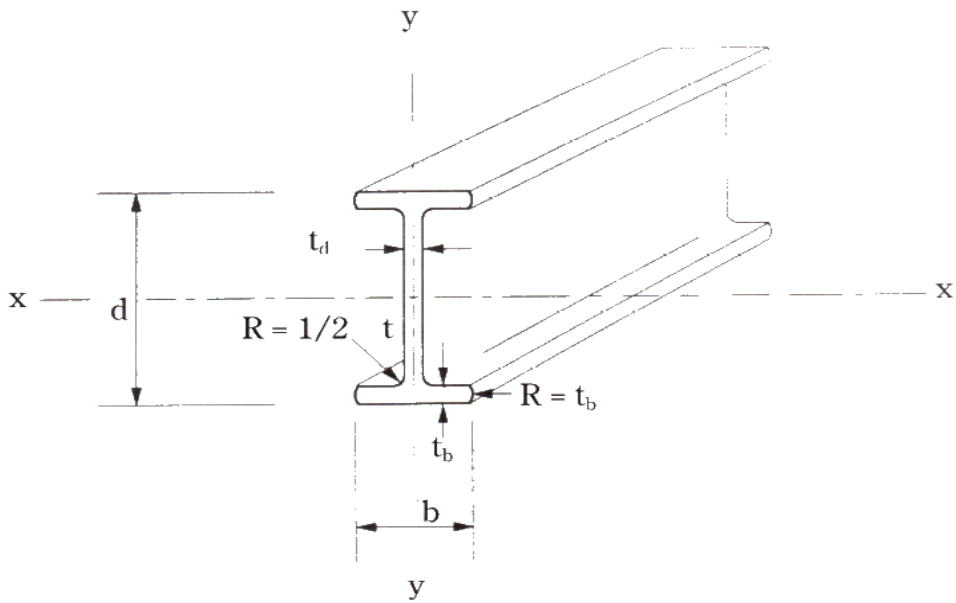
| SECTION DIMENSIONS | | | | | SECTION PROPERTIES | | | | | |
|--------------------|-----|-----|------------------|---------|--------------------|-------|------|--------|-------|------|
| d | b | t | A | Wt | X - X | | | Y - Y | | |
| in. | in. | in. | in. ² | lb./ft. | l | S | r | l | S | r |
| 3 | 3 | 1/4 | 2.13 | 1.64 | 3.17 | 2.11 | 1.22 | 1.13 | 0.75 | 0.73 |
| 4 | 4 | 1/4 | 2.89 | 2.15 | 7.94 | 3.97 | 1.66 | 2.67 | 1.34 | 0.96 |
| 6 | 6 | 1/4 | 4.39 | 3.40 | 28.28 | 9.43 | 2.54 | 9.01 | 3.00 | 1.43 |
| 6 | 6 | 3/8 | 6.48 | 4.90 | 40.17 | 13.39 | 2.49 | 13.52 | 4.51 | 1.44 |
| 8 | 8 | 3/8 | 8.73 | 6.49 | 99.19 | 24.80 | 3.37 | 32.03 | 8.01 | 1.92 |
| 8 | 8 | 1/2 | 11.51 | 8.70 | 126.96 | 31.74 | 3.32 | 42.74 | 10.69 | 1.93 |
| 10 | 10 | 1/2 | 14.51 | 10.90 | 256.20 | 51.24 | 4.21 | 83.42 | 16.68 | 2.40 |
| 12 | 12 | 1/2 | 17.51 | 13.20 | 452.45 | 75.45 | 5.08 | 144.11 | 24.02 | 2.87 |



I-BEAM

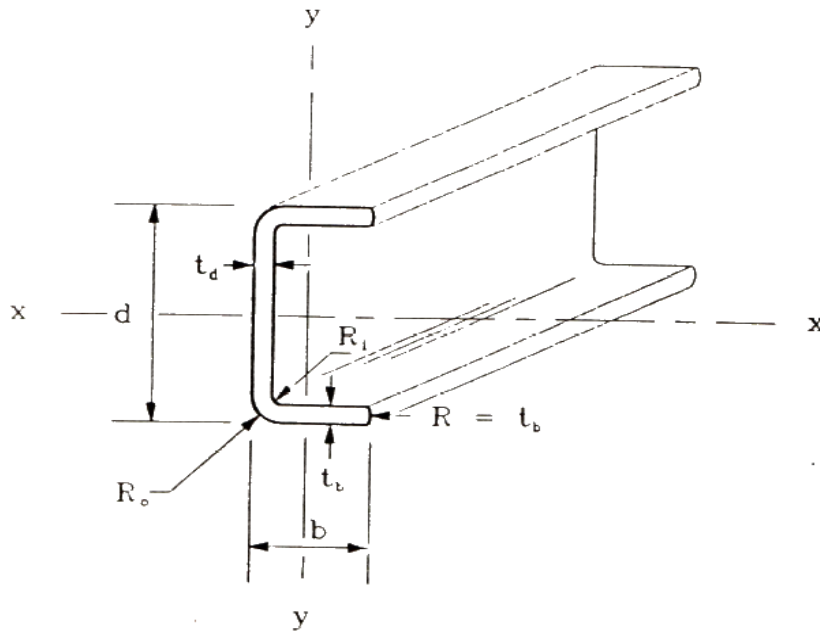
| SECTION DIMENSIONS | | | | | SECTION PROPERTIES | | | | | |
|--------------------|-------|---------|------------------|---------|--------------------|--------|------|-------|-------|------|
| d | b | t | A | Wt | X - X | | | Y - Y | | |
| in. | in. | in. | in. ² | lb./ft. | l | S | r | l | S | r |
| 3 | 1 1/2 | 1/4 | 1.38 | 1.10 | 1.75 | 1.17 | 1.13 | 0.14 | 0.19 | 0.32 |
| 4 | 2 | 1/4 | 1.88 | 1.50 | 4.41 | 2.21 | 1.53 | 0.34 | 0.34 | 0.43 |
| 6 | 3 | 1/4 | 2.88 | 2.20 | 16.99 | 5.66 | 2.43 | 1.13 | 0.75 | 0.63 |
| 6 | 3 | 3/8 | 4.23 | 3.20 | 22.35 | 7.45 | 2.30 | 1.71 | 1.14 | 0.64 |
| 8 | 4 | 3/8 | 5.73 | 4.30 | 55.55 | 13.89 | 3.11 | 4.03 | 2.02 | 0.84 |
| 8 | 4 | 1/2 | 7.51 | 5.70 | 70.62 | 17.66 | 3.07 | 5.40 | 2.70 | 0.85 |
| 10 | 5 | 3/8 | 7.22 | 5.78 | 111.63 | 22.33 | 3.93 | 7.85 | 3.14 | 1.04 |
| 10 | 5 | 1/2 | 9.51 | 7.20 | 143.29 | 28.66 | 3.88 | 10.51 | 4.21 | 1.05 |
| 12 | 6 | 1/2 | 11.51 | 8.70 | 253.96 | 42.33 | 4.70 | 18.11 | 6.04 | 1.26 |
| 18 | 4 1/2 | 3/8-1/2 | 10.92 | 8.70 | 498.15 | 55.35 | 6.75 | 7.66 | 3.40 | 0.84 |
| 24 | 7 1/2 | 3/8-3/4 | 19.90 | 15.20 | 1877.00 | 156.42 | 9.76 | 52.83 | 14.09 | 1.64 |





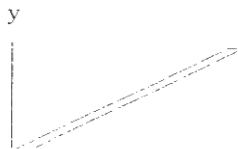
CHANNEL

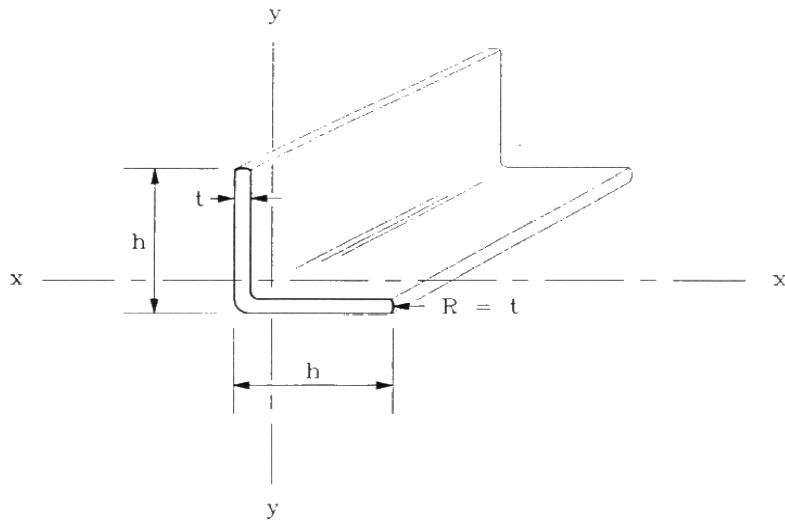
| SECTION DIMENSIONS | | | | | | | | SECTION PROPERTIES | | | | | |
|--------------------|---------|----------------|----------------|------------------|---------|----------------|----------------|--------------------|-------|------|------|------|------|
| d | b | t _d | t _b | A | Wt | R _i | R _o | X-X | | | Y-Y | | |
| in. | in. | in. | in. | in. ² | lb./ft. | in. | in. | I | S | r | I | S | r |
| 3 | 13/16 | 1/8 | 1/8 | 0.55 | 0.43 | 3/16 | 1/32 | 0.64 | 0.43 | 1.08 | 0.03 | 0.04 | 0.22 |
| 3 | 1 | 1/4 | 1/4 | 1.08 | 0.79 | 1/8 | 3/8 | 1.27 | 0.85 | 1.09 | 0.06 | 0.09 | 0.24 |
| 3 | 1 1/2 | 1/4 | 1/4 | 1.33 | 1.01 | 1/8 | 3/8 | 1.75 | 1.16 | 1.15 | 0.26 | 0.25 | 0.44 |
| 3 1/2 | 1 3/16 | 1/8 | 3/16 | 0.88 | 0.67 | 1/8 | 3/16 | 1.54 | 0.88 | 1.32 | 0.11 | 0.13 | 0.36 |
| 4 | 1 1/8 | 1/4 | 1/4 | 1.38 | 1.05 | 1/8 | 3/8 | 2.87 | 1.44 | 1.44 | 0.13 | 0.16 | 0.31 |
| 4 | 1 3/8 | 3/16 | 3/16 | 1.16 | 0.88 | 1/8 | 5/16 | 2.62 | 1.31 | 1.50 | 0.19 | 0.18 | 0.40 |
| 6 | 1 5/8 | 1/4 | 1/4 | 2.13 | 1.67 | 1/8 | 3/8 | 10.18 | 3.39 | 2.19 | 0.43 | 0.35 | 0.45 |
| 6 | 1 11/16 | 3/8 | 3/8 | 3.23 | 2.60 | 1/8 | 1/8 | 14.55 | 4.85 | 2.12 | 0.52 | 0.45 | 0.45 |
| 8 | 2 3/16 | 3/8 | 3/8 | 4.23 | 3.20 | 3/16 | 9/16 | 35.77 | 8.94 | 2.88 | 1.52 | 0.91 | 0.60 |
| 10 | 2 3/4 | 1/2 | 1/2 | 7.02 | 5.30 | 1/4 | 3/4 | 92.49 | 18.50 | 3.63 | 3.97 | 1.92 | 0.75 |



EQUAL LEG ANGLE

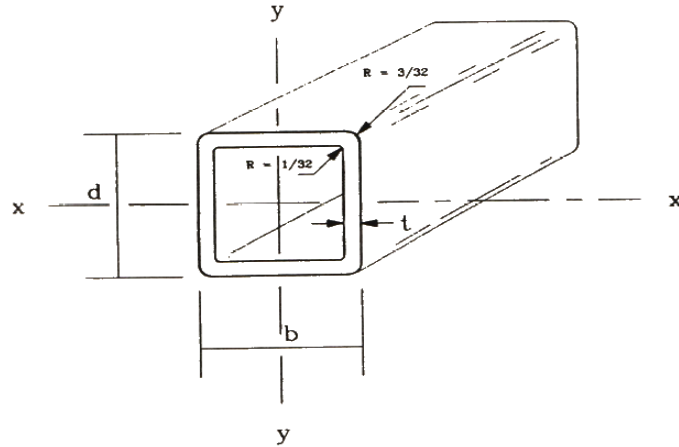
| SECTIONAL DIMENSIONS | | | | SECTIONAL PROPERTIES | | | |
|----------------------|------|------------------|---------|----------------------|------------------|------|------|
| Depth | Wall | A | Wt | X-X / Y-Y | | | |
| h | t | in. ² | lb./ft. | I | S | r | x/y |
| in. | in. | in. ² | lb./ft. | in. ⁴ | in. ³ | in. | in. |
| 1 | 0.13 | 0.23 | 0.18 | 0.02 | 0.05 | 0.31 | 0.29 |
| 1.25 | 0.13 | 0.29 | 0.22 | 0.04 | 0.05 | 0.38 | 0.36 |
| 1.5 | 0.19 | 0.52 | 0.40 | 0.11 | 0.10 | 0.46 | 0.44 |
| 1.5 | 0.25 | 0.67 | 0.54 | 0.14 | 0.13 | 0.45 | 0.47 |
| 2 | 0.25 | 0.92 | 0.70 | 0.33 | 0.23 | 0.59 | 0.59 |
| 3 | 0.25 | 1.42 | 1.08 | 1.24 | 0.58 | 0.93 | 0.84 |
| 3 | 0.38 | 2.09 | 1.61 | 1.76 | 0.83 | 0.91 | 0.89 |
| 3 | 0.50 | 2.70 | 2.11 | 2.22 | 1.07 | 0.91 | 0.93 |
| 4 | 0.25 | 1.92 | 1.45 | 3.04 | 1.04 | 1.26 | 1.09 |
| 4 | 0.38 | 2.84 | 2.18 | 4.35 | 1.52 | 1.24 | 1.14 |
| 4 | 0.50 | 3.70 | 2.89 | 5.56 | 1.97 | 1.23 | 1.18 |
| 6 | 0.50 | 5.70 | 4.45 | 19.91 | 4.60 | 1.87 | 1.68 |





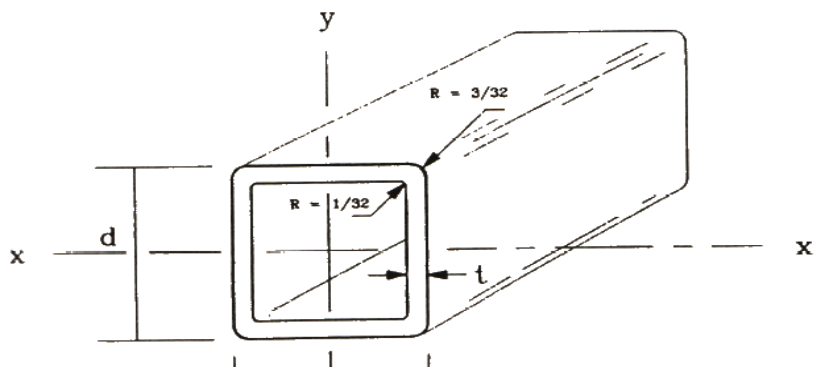
SQUARE TUBE

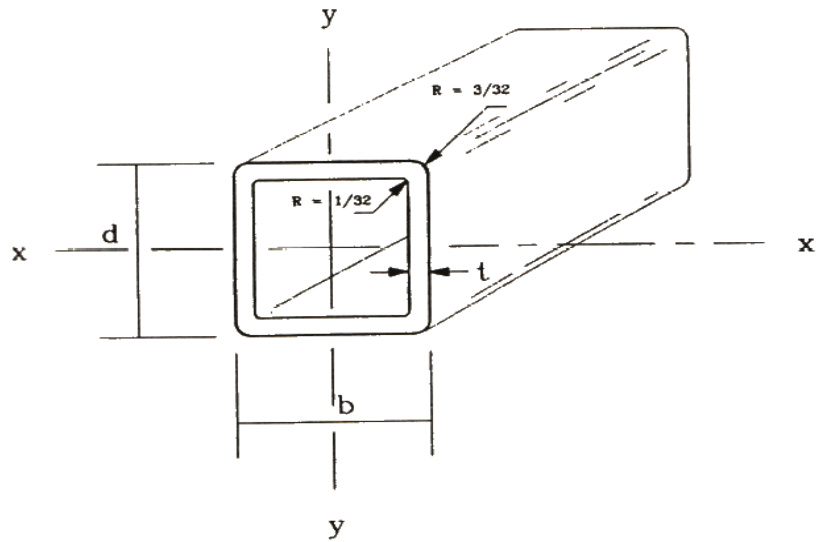
| SECTION DIMENSIONS | | | | SECTION PROPERTIES | | |
|--------------------|-----|------------------|---------|--------------------|------------------|------|
| b | t | A | Wt | I | S | r |
| in. | in. | in. ² | lb./ft. | in. ⁴ | in. ³ | in. |
| 1 | 1/8 | 0.43 | 0.32 | 0.06 | 0.11 | 0.36 |
| 1 | 1/4 | 0.74 | 0.55 | 0.08 | 0.16 | 0.33 |
| 1 1/4 | 1/8 | 0.56 | 0.41 | 0.12 | 0.19 | 0.46 |
| 1 1/4 | 1/4 | 0.99 | 0.75 | 0.18 | 0.28 | 0.42 |
| 1 1/2 | 1/8 | 0.68 | 0.50 | 0.22 | 0.29 | 0.56 |
| 1 1/2 | 1/4 | 1.24 | 0.98 | 0.34 | 0.45 | 0.52 |
| 1 3/4 | 1/8 | 0.81 | 0.61 | 0.36 | 0.41 | 0.67 |
| 1 3/4 | 1/4 | 1.49 | 1.13 | 0.58 | 0.66 | 0.62 |
| 2 | 1/8 | 0.93 | 0.70 | 0.55 | 0.55 | 0.77 |
| 2 | 1/4 | 1.74 | 1.32 | 0.91 | 0.91 | 0.73 |
| 2 | 3/8 | 2.44 | 1.85 | 1.13 | 1.13 | 0.68 |
| 2 1/4 | 1/8 | 1.06 | 0.81 | 0.80 | 0.71 | 0.87 |
| 2 1/4 | 1/4 | 1.99 | 1.51 | 1.35 | 1.20 | 0.83 |
| 3 | 1/8 | 1.43 | 1.08 | 1.98 | 1.32 | 1.18 |
| 3 | 1/4 | 2.74 | 2.07 | 3.50 | 2.33 | 1.13 |
| 4 | 1/4 | 3.74 | 2.83 | 8.82 | 4.41 | 1.53 |



RECTANGULAR TUBE

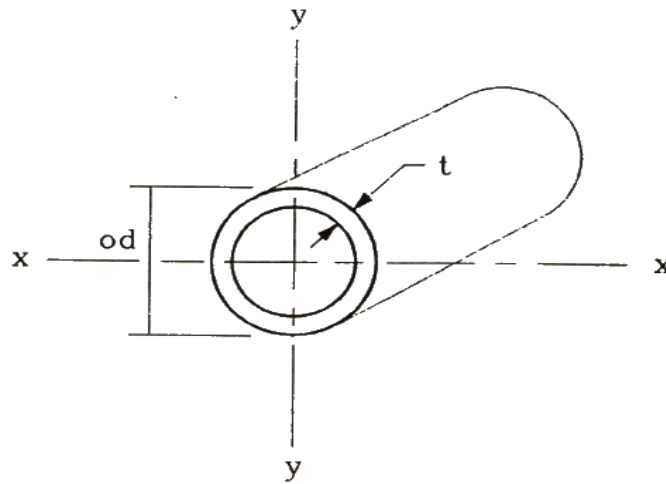
| SECTION DIMENSIONS | | | | | | SECTION PROPERTIES | | | | | |
|--------------------|-------|----------------|----------------|------------------|---------|--------------------|------------------|------|------------------|------------------|------|
| d | b | t _h | t _w | A | Wt | X - X | | | Y - Y | | |
| | | | | | | I | S | r | I | S | r |
| in. | in. | in. | in. | in. ² | lb./ft. | in. ⁴ | in. ³ | in. | in. ⁴ | in. ³ | in. |
| 1 1/2 | 3/4 | 1/8 | 1/8 | 0.50 | 0.39 | 0.13 | 0.17 | 0.51 | 0.04 | 0.11 | 0.32 |
| 1 1/2 | 1 | 1/8 | 1/8 | 0.56 | 0.44 | 0.16 | 0.21 | 0.53 | 0.08 | 0.16 | 0.40 |
| 2 | 1/2 | 1/8 | 1/8 | 0.56 | 0.44 | 0.22 | 0.89 | 0.63 | 0.02 | 0.07 | 0.18 |
| 2 | 1 | 1/8 | 1/8 | 0.69 | 0.54 | 0.33 | 0.33 | 0.69 | 0.11 | 0.21 | 0.39 |
| 4 | 1 | 1/8 | 1/8 | 1.19 | 0.90 | 2.04 | 1.02 | 1.31 | 0.20 | 0.40 | 0.42 |
| 4 3/8 | 1 3/8 | 1/8 | 3/16 | 1.52 | 1.18 | 3.60 | 1.64 | 1.54 | 0.47 | 0.69 | 0.79 |
| 4 1/2 | 1 3/4 | 1/8 | 3/16 | 1.69 | 1.29 | 4.52 | 2.07 | 1.64 | 0.85 | 0.97 | 0.71 |
| 5 | 2 | 1/8 | 1/8 | 1.69 | 1.32 | 5.20 | 2.08 | 1.76 | 1.12 | 1.12 | 0.85 |





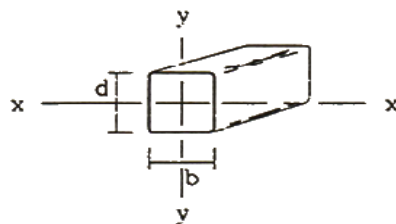
ROUND TUBE

| SECTION DIMENSIONS | | | | SECTION PROPERTIES | | |
|--------------------|------|------------------|---------|--------------------|------------------|------|
| od | t | A | Wt | I | S | r |
| in. | in. | in. ² | lb./ft. | in. ⁴ | in. ³ | in. |
| 1 | 3/32 | 0.27 | 0.22 | 0.03 | 0.06 | 0.32 |
| 1 | 1/8 | 0.34 | 0.25 | 0.03 | 0.07 | 0.31 |
| 1 | 1/8 | 0.39 | 0.33 | 0.05 | 0.09 | 0.36 |
| 1 | 1/4 | 0.34 | 0.27 | 0.06 | 0.09 | 0.41 |
| 1 | 1/4 | 0.44 | 0.32 | 0.07 | 0.11 | 0.40 |
| 1 | 1/4 | 0.79 | 0.61 | 0.10 | 0.17 | 0.36 |
| 1 | 1/2 | 0.54 | 0.45 | 0.13 | 0.17 | 0.49 |
| 1 | 1/2 | 0.98 | 0.79 | 0.20 | 0.27 | 0.45 |
| 1 | 3/4 | 0.64 | 0.51 | 0.21 | 0.24 | 0.58 |
| 1 | 3/4 | 1.18 | 0.94 | 0.34 | 0.39 | 0.54 |
| 1 | 7/8 | 0.99 | 0.88 | 0.36 | 0.38 | 0.60 |
| 2 | 1/4 | 1.37 | 1.08 | 0.54 | 0.54 | 0.62 |
| 3 | 1/4 | 2.16 | 1.70 | 2.06 | 1.37 | 0.98 |
| 3 | 1/2 | 3.93 | 2.98 | 3.19 | 2.13 | 0.90 |



SQUARE BAR

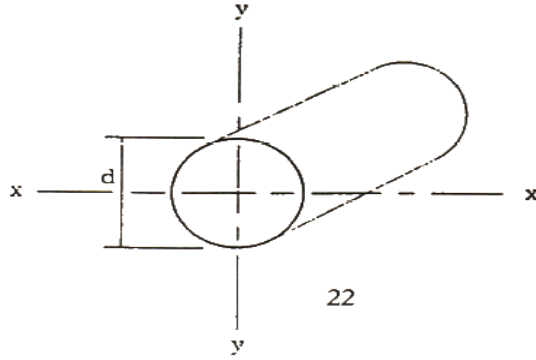
| SECTION DIMENSIONS | | | | SECTION PROPERTIES | | | | | |
|--------------------|-------|------------------|---------|--------------------|------------------|------|------------------|------------------|------|
| d | b | A | Wt | X - X | | | Y - Y | | |
| | | | | I | S | r | I | S | r |
| in. | in. | in. ² | lb./ft. | in. ⁴ | in. ³ | in. | in. ⁴ | in. ³ | in. |
| 1 | 1 | 1.00 | 0.88 | 0.08 | 0.17 | 0.29 | 0.08 | 0.17 | 0.29 |
| 1 1/4 | 1 1/4 | 1.56 | 1.37 | 0.20 | 0.33 | 0.36 | 0.20 | 0.33 | 0.36 |
| 1 1/2 | 1 1/2 | 2.25 | 1.98 | 0.42 | 0.56 | 0.43 | 0.42 | 0.56 | 0.43 |



|b|
y

SOLID ROUND

| SECTION DIMENSIONS | | | SECTION PROPERTIES | | |
|--------------------|------------------|---------|--------------------|------------------|--------|
| d | A | Wt | I | S | r |
| in. | in. ² | lb./ft. | in. ⁴ | in. ³ | in. |
| 0.2500 | 0.049 | 0.044 | 0.0002 | 0.0016 | 0.0625 |
| 0.3000 | 0.071 | 0.062 | 0.0004 | 0.0027 | 0.0750 |
| 0.3125 | 0.077 | 0.067 | 0.0005 | 0.0030 | 0.0781 |
| 0.3500 | 0.096 | 0.083 | 0.0007 | 0.0042 | 0.0875 |
| 0.3750 | 0.110 | 0.095 | 0.0010 | 0.0052 | 0.0938 |
| 0.4375 | 0.150 | 0.133 | 0.0018 | 0.0082 | 0.1094 |
| 0.4720 | 0.175 | 0.150 | 0.0024 | 0.0103 | 0.1180 |
| 0.4800 | 0.181 | 0.160 | 0.0026 | 0.0109 | 0.1200 |
| 0.5000 | 0.196 | 0.172 | 0.0031 | 0.0123 | 0.1250 |
| 0.6250 | 0.307 | 0.270 | 0.0075 | 0.0240 | 0.1563 |
| 0.7500 | 0.442 | 0.397 | 0.0156 | 0.0414 | 0.1875 |
| 0.8125 | 0.518 | 0.460 | 0.0214 | 0.0527 | 0.2031 |
| 0.8750 | 0.601 | 0.534 | 0.0288 | 0.0658 | 0.2188 |
| 1.0000 | 0.785 | 0.697 | 0.0491 | 0.0982 | 0.2500 |
| 1.2500 | 1.227 | 1.094 | 0.1198 | 0.1917 | 0.3125 |
| 1.5000 | 1.766 | 1.571 | 0.2485 | 0.3313 | 0.3750 |



ALLOWABLE UNIFORM LOAD TABLE NOTATION

- A_w - Area of web (in²)
! - Deflection (in)
E - Modulus of Elasticity (psi)
 F_b - Maximum Allowable Flexural Stress for Laterally Supported Beam (psi)
 F_v - Maximum Allowable Shear Stress for Laterally Supported Beam (psi)
G - Shear Modulus (psi)
I - Moment of Inertia (in⁴)
L - Span Length (in)
S - Section Modulus (in³)
V - Vertical Shear (lbs)
w - Uniform Load (lbs/in)
M - Maximum Moment (in-lb)

The allowable uniform load tables were generated using the results from tests and the following formulas, properties, and assumptions. The Deflection formula reflects that the deflection is the result of both flexural and shear stresses.

$$! = \frac{5wL^4}{384EI} + \frac{wL^2}{4A_wG}$$

$$F_v = \frac{V}{A_w}$$

$$F_b = \frac{M}{S}$$

$$E = 2.8 \times 10^6 \text{ psi}$$

$$G = 450,000 \text{ psi}$$

$$F_b = 10,000 \text{ psi}$$

$$F_v = 1,500 \text{ psi}$$

Adequate lateral support is provided (full lateral support for channels).

Load is applied perpendicular to major axis.

Beam simply supported at both ends.

The part weight has been deduced in the following tables.

**ALLOWABLE UNIFORM LOADS (lbs./ft.)
Laterally Supported**

3 X 3 X 1/4 WIDE FLANGE BEAM
 $A_w=0.625 \text{ in}^2$ $I_x=3.17 \text{ in}^4$ $S_x=2.11 \text{ in}^3$ $Wt.=1.64 \text{ lbs./ft}$

| SPAN FEET | MAXIMUM LOAD | | DEFLECTION | | | | |
|-----------|--------------|-------|------------|-------|-------|-------|-------|
| | | | L/100 | L/150 | L/180 | L/240 | L/360 |
| 3 | 623 | F_v | * | * | * | 496 | 330 |
| 4 | 467 | F_v | * | 388 | 323 | 242 | 161 |
| 5 | 373 | F_v | 322 | 214 | 178 | 133 | 88 |
| 6 | 311 | F_v | 194 | 129 | 107 | 80 | 53 |
| 7 | 266 | F_v | 125 | 83 | 69 | 51 | 33 |
| 8 | 218 | F_v | 85 | 56 | 46 | 34 | 22 |
| 9 | 172 | F_v | 60 | 39 | 32 | 24 | 15 |
| 10 | 139 | F_v | 43 | 28 | 23 | 17 | 11 |

The part weight has been deduced in the above table

4 X 4 X 1/4 WIDE FLANGE BEAM
 $A_w=0.875 \text{ in}^2$ $I_x=7.94 \text{ in}^4$ $S_x=3.97 \text{ in}^3$ $Wt.=2.15 \text{ lbs./ft}$

| SPAN FEET | MAXIMUM LOAD | | DEFLECTION | | | | |
|-----------|--------------|-------|------------|-------|-------|-------|-------|
| | | | L/100 | L/150 | L/180 | L/240 | L/360 |
| 3 | 872 | F_v | * | * | * | * | 661 |
| 4 | 653 | F_v | * | * | * | 522 | 347 |
| 5 | 522 | F_v | * | 483 | 402 | 301 | 200 |
| 6 | 435 | F_v | * | 300 | 249 | 186 | 123 |
| 7 | 372 | F_v | 297 | 197 | 163 | 122 | 80 |
| 8 | 325 | F_v | 204 | 135 | 112 | 83 | 55 |
| 9 | 289 | F_v | 146 | 96 | 80 | 59 | 38 |
| 10 | 260 | F_v | 107 | 71 | 58 | 43 | 28 |
| 11 | 216 | F_b | 81 | 53 | 44 | 32 | 20 |
| 12 | 181 | F_b | 62 | 40 | 33 | 24 | 15 |
| 13 | 154 | F_b | 49 | 31 | 26 | 19 | 11 |

The part weight has been deduced in the above table

6 X 6 X 1/4 WIDE FLANGE BEAM
 $A_w=1.375 \text{ in}^2$ $I_x=28.28 \text{ in}^4$ $S_x=9.43 \text{ in}^3$ $Wt.=3.40 \text{ lbs./ft}$

| SPAN FEET | MAXIMUM LOAD | | DEFLECTION | | | | |
|-----------|--------------|----------------|------------|-------|-------|-------|-------|
| | | | L/100 | L/150 | L/180 | L/240 | L/360 |
| 5 | 821 | F _v | * | * | * | * | 554 |
| 6 | 684 | F _v | * | * | * | 549 | 364 |
| 7 | 585 | F _v | * | * | 503 | 377 | 250 |
| 8 | 512 | F _v | * | 430 | 358 | 267 | 177 |
| 9 | 454 | F _v | * | 315 | 262 | 195 | 129 |
| 10 | 409 | F _v | 357 | 237 | 196 | 146 | 96 |
| 11 | 371 | F _v | 274 | 181 | 150 | 112 | 73 |
| 12 | 450 | F _v | 215 | 142 | 117 | 87 | 57 |
| 13 | 313 | F _v | 171 | 112 | 93 | 69 | 44 |
| 14 | 219 | F _v | 138 | 90 | 75 | 55 | 35 |
| 15 | 271 | F _v | 112 | 74 | 61 | 44 | 28 |

The part weight has been deduced in the above table

6 X 6 X 3/8 WIDE FLANGE BEAM
 $A_w=1.969 \text{ in}^2$ $I_x=40.17 \text{ in}^4$ $S_x=13.39 \text{ in}^3$ $Wt.=4.90 \text{ lbs./ft}$

| SPAN FEET | MAXIMUM LOAD | | DEFLECTION | | | | |
|-----------|--------------|----------------|------------|-------|-------|-------|-------|
| | | | L/100 | L/150 | L/180 | L/240 | L/360 |
| 5 | 1176 | F _v | * | * | * | * | 790 |
| 6 | 980 | F _v | * | * | * | 782 | 520 |
| 7 | 839 | F _v | * | * | 717 | 537 | 356 |
| 8 | 733 | F _v | * | 613 | 510 | 381 | 252 |
| 9 | 651 | F _v | * | 449 | 373 | 279 | 184 |
| 10 | 586 | F _v | 508 | 337 | 280 | 209 | 138 |
| 11 | 532 | F _v | 390 | 259 | 215 | 160 | 105 |
| 12 | 487 | F _v | 306 | 202 | 168 | 124 | 81 |
| 13 | 449 | F _v | 243 | 160 | 133 | 98 | 64 |
| 14 | 417 | F _v | 196 | 129 | 107 | 79 | 51 |
| 15 | 389 | F _v | 160 | 0.5 | 87 | 64 | 41 |

The part weight has been deduced in the above table

8 X 8 X 3/8 WIDE FLANGE BEAM
 $A_w=2.719 \text{ in}^2$ $I_x=99.18 \text{ in}^4$ $S_x=24.80 \text{ in}^3$ $Wt.=6.49 \text{ lbs./ft}$

| SPAN FEET | MAXIMUM LOAD | | DEFLECTION | | | | |
|-----------|--------------|----------------|------------|-------|-------|-------|-------|
| | | | L/100 | L/150 | L/180 | L/240 | L/360 |
| 6 | 1353 | F _v | * | * | * | * | 1028 |
| 7 | 1158 | F _v | * | * | * | 1105 | 735 |
| 8 | 1013 | F _v | * | * | * | 811 | 539 |
| 9 | 899 | F _v | * | * | 815 | 609 | 404 |
| 10 | 809 | F _v | * | 751 | 625 | 467 | 309 |
| 11 | 735 | F _v | * | 586 | 488 | 364 | 240 |
| 12 | 673 | F _v | * | 465 | 387 | 288 | 190 |
| 13 | 620 | F _v | 565 | 374 | 311 | 231 | 152 |
| 14 | 576 | F _v | 461 | 305 | 253 | 188 | 123 |
| 15 | 537 | F _v | 380 | 251 | 208 | 154 | 100 |
| 16 | 503 | F _v | 316 | 209 | 173 | 128 | 83 |
| 17 | 473 | F _v | 266 | 175 | 145 | 107 | 69 |
| 18 | 446 | F _v | 225 | 148 | 122 | 90 | 58 |
| 19 | 422 | F _v | 192 | 126 | 104 | 76 | 48 |
| 20 | 401 | F _v | 165 | 108 | 89 | 65 | 41 |
| 21 | 368 | F _b | 143 | 93 | 76 | 55 | 35 |
| 22 | 335 | F _b | 124 | 80 | 66 | 48 | 29 |
| 23 | 306 | F _b | 108 | 70 | 57 | 41 | 25 |
| 24 | 280 | F _b | 95 | 61 | 50 | 35 | 21 |
| 25 | 258 | F _b | 83 | 53 | 43 | 31 | 18 |

The part weight has been deduced in the above table

8 X 8 X 1/2 WIDE FLANGE BEAM
 $A_w=3.500 \text{ in}^2$ $I_x=126.96 \text{ in}^4$ $S_x=31.74 \text{ in}^3$ $Wt.=8.70 \text{ lbs./ft}$

| SPAN FEET | MAXIMUM LOAD | | DEFLECTION | | | | |
|--------------|--------------|----------------|------------|-------|-------|-------|-------|
| | | | L/100 | L/150 | L/180 | L/240 | L/360 |
| 6 | 1741 | F _v | * | * | * | * | 1319 |
| 7 | 1491 | F _v | * | * | * | 1418 | 942 |
| 8 | 1304 | F _v | * | * | * | 1040 | 691 |
| 9 | 1158 | F _v | * | * | 1044 | 781 | 518 |
| 10 | 1041 | F _v | * | 963 | 801 | 598 | 396 |
| 11 | 946 | F _v | * | 751 | 625 | 466 | 308 |
| 12 | 866 | F _v | * | 596 | 495 | 369 | 243 |
| 13 | 799 | F _v | 724 | 479 | 398 | 296 | 194 |
| 14 | 741 | F _v | 590 | 390 | 324 | 241 | 157 |
| 15 | 691 | F _v | 486 | 321 | 266 | 197 | 129 |
| 16 | 647 | F _v | 405 | 267 | 221 | 164 | 106 |
| 17 | 609 | F _v | 341 | 224 | 185 | 137 | 88 |
| 18 | 574 | F _v | 288 | 189 | 156 | 115 | 74 |
| 19 | 544 | F _v | 246 | 161 | 133 | 97 | 62 |
| 20 | 516 | F _v | 211 | 138 | 113 | 83 | 52 |
| 21 | 471 | F _b | 183 | 119 | 97 | 71 | 44 |
| 22 | 428 | F _b | 159 | 103 | 84 | 61 | 38 |
| 23 | 391 | F _b | 138 | 89 | 73 | 52 | 32 |
| 24 | 385 | F _b | 121 | 78 | 63 | 45 | 27 |
| 25 | 330 | F _b | 107 | 68 | 55 | 39 | 23 |

The part weight has been deduced in the above table

10 X 10 X 1/2 WIDE FLANGE BEAM
 $A_w=4.500 \text{ in}^2$ $I_x=256.20 \text{ in}^4$ $S_x=51.24 \text{ in}^3$ $Wt.=10.90 \text{ lbs./ft}$

| SPAN FEET | MAXIMUM LOAD | | DEFLECTION | | | | |
|-----------|--------------|----------------|------------|-------|-------|-------|-------|
| | | | L/100 | L/150 | L/180 | L/240 | L/360 |
| 7 | 1918 | F _v | * | * | * | * | 1567 |
| 8 | 1677 | F _v | * | * | * | * | 1183 |
| 9 | 1489 | F _v | * | * | * | 1370 | 910 |
| 10 | 1339 | F _v | * | * | * | 1072 | 711 |
| 11 | 1216 | F _v | * | * | 1138 | 850 | 563 |
| 12 | 1114 | F _v | * | 1100 | 915 | 684 | 452 |
| 13 | 1027 | F _v | * | 896 | 745 | 556 | 367 |
| 14 | 953 | F _v | * | 738 | 613 | 457 | 301 |
| 15 | 889 | F _v | * | 614 | 510 | 379 | 249 |
| 16 | 833 | F _v | 778 | 515 | 427 | 318 | 208 |
| 17 | 783 | F _v | 658 | 435 | 361 | 268 | 175 |
| 18 | 739 | F _v | 562 | 371 | 307 | 228 | 148 |
| 19 | 700 | F _v | 482 | 318 | 263 | 195 | 126 |
| 20 | 664 | F _v | 417 | 274 | 227 | 167 | 108 |
| 21 | 632 | F _v | 362 | 238 | 196 | 144 | 93 |
| 22 | 603 | F _v | 316 | 207 | 171 | 125 | 80 |
| 23 | 576 | F _v | 278 | 181 | 149 | 109 | 69 |
| 24 | 552 | F _v | 245 | 160 | 131 | 96 | 60 |
| 25 | 529 | F _v | 217 | 141 | 115 | 84 | 52 |
| 26 | 494 | F _b | 192 | 125 | 102 | 74 | 46 |
| 27 | 458 | F _b | 172 | 111 | 90 | 65 | 40 |
| 28 | 425 | F _b | 153 | 99 | 80 | 57 | 35 |
| 29 | 395 | F _b | 138 | 88 | 72 | 51 | 30 |
| 30 | 369 | F _b | 124 | 79 | 64 | 45 | 26 |

The part weight has been deduced in the above table

12 X 12 X 1/2 WIDE FLANGE BEAM
 $A_w=5.500 \text{ in}^2$ $I_x=452.45 \text{ in}^4$ $S_x=75.45 \text{ in}^3$ $Wt.=13.20 \text{ lbs./ft}$

| SPAN FEET | MAXIMUM LOAD | | DEFLECTION | | | | |
|-----------|--------------|----------------|------------|-------|-------|-------|-------|
| | | | L/100 | L/150 | L/180 | L/240 | L/360 |
| 7 | 2343 | F _v | * | * | * | * | 2273 |
| 8 | 2049 | F _v | * | * | * | * | 1760 |
| 9 | 1819 | F _v | * | * | * | * | 1383 |
| 10 | 1636 | F _v | * | * | * | * | 1102 |
| 11 | 1486 | F _v | * | * | * | 1338 | 888 |
| 12 | 1361 | F _v | * | * | * | 1091 | 723 |
| 13 | 1255 | F _v | * | * | 1203 | 899 | 595 |
| 14 | 1165 | F _v | * | * | 1001 | 747 | 493 |
| 15 | 1086 | F _v | * | 1010 | 839 | 626 | 413 |
| 16 | 1017 | F _v | * | 854 | 710 | 529 | 348 |
| 17 | 957 | F _v | * | 728 | 604 | 450 | 295 |
| 18 | 903 | F _v | * | 624 | 518 | 385 | 252 |
| 19 | 854 | F _v | 814 | 538 | 446 | 331 | 216 |
| 20 | 811 | F _v | 707 | 467 | 387 | 287 | 186 |
| 21 | 772 | F _v | 618 | 407 | 337 | 249 | 161 |
| 22 | 736 | F _v | 542 | 357 | 295 | 218 | 140 |
| 23 | 703 | F _v | 478 | 314 | 259 | 191 | 123 |
| 24 | 674 | F _v | 423 | 277 | 229 | 168 | 107 |
| 25 | 646 | F _v | 376 | 246 | 203 | 148 | 94 |
| 26 | 621 | F _v | 335 | 219 | 180 | 131 | 83 |
| 27 | 597 | F _v | 300 | 195 | 160 | 117 | 73 |
| 28 | 575 | F _v | 269 | 175 | 143 | 104 | 65 |
| 29 | 555 | F _v | 242 | 157 | 128 | 93 | 57 |
| 30 | 536 | F _v | 219 | 141 | 115 | 83 | 51 |

The part weight has been deduced in the above table

3 X 1-1/2 X 1/2 I-BEAM
 $A_w=0.625 \text{ in}^2$ $I_x=1.75 \text{ in}^4$ $S_x=1.17 \text{ in}^3$ $Wt.=1.10 \text{ lbs./ft}$

| SPAN FEET | MAXIMUM LOAD | | DEFLECTION | | | | |
|-----------|--------------|----------------|------------|-------|-------|-------|-------|
| | | | L/100 | L/150 | L/180 | L/240 | L/360 |
| 3 | 623 | F _v | * | 511 | 425 | 319 | 212 |
| 4 | 467 | F _v | 355 | 236 | 196 | 147 | 97 |
| 5 | 310 | F _b | 189 | 126 | 104 | 78 | 51 |
| 6 | 215 | F _b | 112 | 74 | 61 | 45 | 30 |
| 7 | 157 | F _b | 71 | 46 | 38 | 28 | 18 |
| 8 | 120 | F _b | 47 | 31 | 25 | 19 | 12 |
| 9 | 94 | F _b | 33 | 21 | 17 | 13 | 8 |
| 10 | 76 | F _b | 24 | 15 | 12 | 9 | 5 |

The part weight has been deduced in the above table

4 X 2 X 1/4 I-BEAM
 $A_w=0.875 \text{ in}^2$ $I_x=4.41 \text{ in}^4$ $S_x=2.21 \text{ in}^3$ $Wt.=1.50 \text{ lbs./ft}$

| SPAN FEET | MAXIMUM LOAD | | DEFLECTION | | | | |
|-----------|--------------|----------------|------------|-------|-------|-------|-------|
| | | | L/100 | L/150 | L/180 | L/240 | L/360 |
| 3 | 873 | F _v | * | * | * | 692 | 461 |
| 4 | 654 | F _v | * | 542 | 451 | 338 | 225 |
| 5 | 523 | F _v | 449 | 299 | 249 | 186 | 123 |
| 6 | 407 | F _b | 271 | 180 | 150 | 112 | 74 |
| 7 | 299 | F _b | 175 | 116 | 96 | 72 | 47 |
| 8 | 228 | F _b | 119 | 78 | 65 | 48 | 32 |
| 9 | 180 | F _b | 84 | 55 | 46 | 34 | 22 |
| 10 | 145 | F _b | 61 | 40 | 33 | 24 | 16 |
| 11 | 120 | F _b | 46 | 30 | 25 | 18 | 11 |
| 12 | 100 | F _b | 35 | 23 | 19 | 13 | 8 |

The part weight has been deduced in the above table

6 X 3 X 1/4 I-BEAM
 $A_w=1.375 \text{ in}^2$ $I_x=16.99 \text{ in}^4$ $S_x=5.66 \text{ in}^3$ $Wt.=2.20 \text{ lbs./ft}$

| SPAN FEET | MAXIMUM LOAD | | DEFLECTION | | | | |
|-----------|--------------|----------------|------------|-------|-------|-------|-------|
| | | | L/100 | L/150 | L/180 | L/240 | L/360 |
| 5 | 822 | F _v | * | * | 797 | 597 | 397 |
| 6 | 685 | F _v | * | 607 | 505 | 378 | 251 |
| 7 | 586 | F _v | * | 405 | 337 | 252 | 167 |
| 8 | 513 | F _v | 424 | 282 | 234 | 175 | 116 |
| 9 | 455 | F _v | 306 | 203 | 169 | 126 | 83 |
| 10 | 374 | F _b | 227 | 150 | 125 | 93 | 61 |
| 11 | 309 | F _b | 173 | 114 | 95 | 70 | 46 |
| 12 | 259 | F _b | 134 | 88 | 73 | 54 | 35 |
| 13 | 220 | F _b | 106 | 70 | 57 | 42 | 27 |
| 14 | 189 | F _b | 85 | 56 | 46 | 34 | 21 |
| 15 | 165 | F _b | 69 | 45 | 37 | 27 | 17 |

The part weight has been deduced in the above table

6 X 3 X 3/8 I-BEAM
 $A_w=1.969 \text{ in}^2$ $I_x=22.35 \text{ in}^4$ $S_x=7.45 \text{ in}^3$ $Wt.=3.20 \text{ lbs./ft}$

| SPAN FEET | MAXIMUM LOAD | | DEFLECTION | | | | |
|-----------|--------------|----------------|------------|-------|-------|-------|-------|
| | | | L/100 | L/150 | L/180 | L/240 | L/360 |
| 6 | 981 | F _v | * | 813 | 676 | 506 | 336 |
| 7 | 840 | F _v | 812 | 540 | 449 | 336 | 223 |
| 8 | 734 | F _v | 564 | 375 | 312 | 233 | 154 |
| 9 | 609 | F _b | 406 | 269 | 224 | 167 | 110 |
| 10 | 493 | F _b | 301 | 199 | 165 | 123 | 81 |
| 11 | 406 | F _b | 229 | 151 | 125 | 93 | 61 |
| 12 | 341 | F _b | 177 | 117 | 97 | 72 | 46 |
| 13 | 290 | F _b | 140 | 92 | 76 | 56 | 36 |
| 14 | 249 | F _b | 112 | 73 | 60 | 44 | 28 |
| 15 | 217 | F _b | 91 | 59 | 49 | 36 | 22 |
| 16 | 190 | F _b | 75 | 48 | 40 | 29 | 18 |
| 17 | 168 | F _b | 62 | 40 | 33 | 23 | 14 |
| 18 | 149 | F _b | 52 | 33 | 27 | 19 | 11 |

The part weight has been deduced in the above table

8 X 4 X 3/8 I-BEAM
 $A_w=2.719 \text{ in}^2$ $I_x=55.55 \text{ in}^4$ $S_x=13.89 \text{ in}^3$ $Wt.=4.30 \text{ lbs./ft}$

| SPAN FEET | MAXIMUM LOAD | | DEFLECTION | | | | |
|-----------|--------------|----------------|------------|-------|-------|-------|-------|
| | | | L/100 | L/150 | L/180 | L/240 | L/360 |
| 6 | 1355 | F _v | * | * | * | 1083 | 720 |
| 7 | 1160 | F _v | * | * | 993 | 744 | 494 |
| 8 | 1015 | F _v | * | 849 | 707 | 529 | 351 |
| 9 | 901 | F _v | * | 622 | 518 | 387 | 256 |
| 10 | 811 | F _v | 704 | 468 | 389 | 291 | 192 |
| 11 | 737 | F _v | 542 | 359 | 299 | 223 | 147 |
| 12 | 638 | F _b | 425 | 281 | 234 | 174 | 114 |
| 13 | 543 | F _b | 338 | 224 | 186 | 138 | 90 |
| 14 | 467 | F _b | 273 | 181 | 150 | 111 | 72 |
| 15 | 407 | F _b | 224 | 147 | 122 | 90 | 58 |
| 16 | 357 | F _b | 185 | 122 | 101 | 74 | 48 |
| 17 | 315 | F _b | 154 | 101 | 84 | 61 | 39 |
| 18 | 281 | F _b | 130 | 85 | 70 | 51 | 33 |
| 19 | 251 | F _b | 111 | 72 | 59 | 43 | 27 |
| 20 | 226 | F _b | 94 | 61 | 50 | 36 | 23 |

The part weight has been deduced in the above table

8 X 4 X 1/2 I-BEAM
 $A_w=3.500 \text{ in}^2$ $I_x=70.62 \text{ in}^4$ $S_x=17.66 \text{ in}^3$ $Wt.=5.70 \text{ lbs./ft}$

| SPAN FEET | MAXIMUM LOAD | | DEFLECTION | | | | |
|-----------|--------------|----------------|------------|-------|-------|-------|-------|
| | | | L/100 | L/150 | L/180 | L/240 | L/360 |
| 6 | 1744 | F _v | * | * | * | 1383 | 920 |
| 7 | 1494 | F _v | * | * | 1267 | 949 | 631 |
| 8 | 1307 | F _v | * | 1082 | 901 | 674 | 448 |
| 9 | 1161 | F _v | * | 793 | 660 | 494 | 327 |
| 10 | 1044 | F _v | 897 | 596 | 496 | 370 | 245 |
| 11 | 949 | F _v | 690 | 458 | 381 | 284 | 187 |
| 12 | 812 | F _b | 541 | 358 | 298 | 222 | 146 |
| 13 | 691 | F _b | 431 | 285 | 237 | 176 | 115 |
| 14 | 595 | F _b | 348 | 230 | 191 | 142 | 92 |
| 15 | 517 | F _b | 285 | 188 | 156 | 115 | 75 |
| 16 | 454 | F _b | 236 | 155 | 128 | 95 | 61 |
| 17 | 401 | F _b | 197 | 129 | 107 | 79 | 50 |
| 18 | 357 | F _b | 166 | 109 | 90 | 66 | 42 |
| 19 | 320 | F _b | 141 | 92 | 76 | 55 | 35 |
| 20 | 288 | F _b | 121 | 78 | 64 | 47 | 29 |

The part weight has been deduced in the above table

10 X 5 X 1/2 I-BEAM
 $A_w=4.500 \text{ in}^2$ $I_x=143.29 \text{ in}^4$ $S_x=28.66 \text{ in}^3$ $Wt.=7.20 \text{ lbs./ft}$

| SPAN FEET | MAXIMUM LOAD | | DEFLECTION | | | | |
|-----------|--------------|----------------|------------|-------|-------|-------|-------|
| | | | L/100 | L/150 | L/180 | L/240 | L/360 |
| 6 | 2242 | F _v | * | * | * | * | 1579 |
| 7 | 1921 | F _v | * | * | * | 1681 | 1118 |
| 8 | 1680 | F _v | * | * | 1635 | 1225 | 814 |
| 9 | 1492 | F _v | * | 1468 | 1222 | 914 | 607 |
| 10 | 1342 | F _v | * | 1120 | 932 | 697 | 462 |
| 11 | 1219 | F _v | * | 872 | 725 | 542 | 359 |
| 12 | 1117 | F _v | 1038 | 690 | 573 | 428 | 283 |
| 13 | 1030 | F _v | 834 | 554 | 460 | 343 | 226 |
| 14 | 956 | F _v | 679 | 450 | 374 | 278 | 183 |
| 15 | 841 | F _b | 599 | 370 | 307 | 228 | 150 |
| 16 | 738 | F _b | 466 | 308 | 255 | 189 | 124 |
| 17 | 653 | F _b | 391 | 258 | 214 | 158 | 103 |
| 18 | 582 | F _b | 331 | 218 | 180 | 133 | 86 |
| 19 | 521 | F _b | 283 | 186 | 153 | 113 | 73 |
| 20 | 470 | F _b | 243 | 159 | 131 | 97 | 62 |
| 21 | 425 | F _b | 210 | 137 | 113 | 83 | 53 |
| 22 | 387 | F _b | 183 | 119 | 98 | 71 | 45 |
| 23 | 353 | F _b | 160 | 104 | 85 | 62 | 39 |
| 24 | 324 | F _b | 140 | 91 | 74 | 54 | 33 |
| 25 | 298 | F _b | 123 | 80 | 65 | 47 | 28 |

The part weight has been deduced in the above table

10 X 5 X 3/8 I-BEAM
 $A_w=3.469 \text{ in}^2$ $I_x=111.63 \text{ in}^4$ $S_x=22.33 \text{ in}^3$ $Wt.=5.78 \text{ lbs./ft}$

| SPAN FEET | MAXIMUM LOAD | | DEFLECTION | | | | |
|-----------|--------------|----------------|------------|-------|-------|-------|-------|
| | | | L/100 | L/150 | L/180 | L/240 | L/360 |
| 6 | 1728 | F _v | * | * | * | * | 1225 |
| 7 | 1481 | F _v | * | * | * | 1305 | 868 |
| 8 | 1295 | F _v | * | * | 1270 | 951 | 632 |
| 9 | 1150 | F _v | * | 1141 | 949 | 711 | 472 |
| 10 | 1035 | F _v | * | 871 | 725 | 542 | 359 |
| 11 | 940 | F _v | * | 678 | 564 | 422 | 279 |
| 12 | 861 | F _v | 808 | 537 | 446 | 333 | 220 |
| 13 | 794 | F _v | 649 | 431 | 358 | 267 | 176 |
| 14 | 737 | F _v | 529 | 350 | 291 | 217 | 143 |
| 15 | 656 | F _b | 436 | 288 | 239 | 178 | 117 |
| 16 | 575 | F _b | 363 | 240 | 199 | 148 | 96 |
| 17 | 509 | F _b | 305 | 201 | 167 | 123 | 80 |
| 18 | 453 | F _b | 258 | 170 | 141 | 104 | 67 |
| 19 | 406 | F _b | 220 | 145 | 120 | 88 | 57 |
| 20 | 366 | F _b | 189 | 124 | 103 | 75 | 48 |
| 21 | 332 | F _b | 164 | 107 | 88 | 65 | 41 |
| 22 | 302 | F _b | 142 | 93 | 76 | 56 | 35 |
| 23 | 275 | F _b | 124 | 81 | 66 | 48 | 30 |
| 24 | 252 | F _b | 109 | 71 | 58 | 42 | 26 |
| 25 | 232 | F _b | 96 | 62 | 51 | 37 | 22 |

The part weight has been deduced in the above table

12 X 6 X 1/2 I-BEAM
 $A_w=5.50 \text{ in}^2$ $I_x=253.96 \text{ in}^4$ $S_x=42.33 \text{ in}^3$ $Wt.=8.70 \text{ lbs./ft}$

| SPAN FEET | MAXIMUM LOAD | | DEFLECTION | | | | |
|--------------|--------------|----------------|------------|-------|-------|-------|-------|
| | | | L/100 | L/150 | L/180 | L/240 | L/360 |
| 6 | 2741 | F _v | * | * | * | * | 3254 |
| 7 | 2348 | F _v | * | * | * | * | 1715 |
| 8 | 2054 | F _v | * | * | * | 1922 | 1278 |
| 9 | 1824 | F _v | * | * | * | 1463 | 972 |
| 10 | 1641 | F _v | * | * | 1514 | 1134 | 753 |
| 11 | 1491 | F _v | * | 1434 | 1193 | 893 | 592 |
| 12 | 1366 | F _v | * | 1147 | 954 | 713 | 473 |
| 13 | 1260 | F _v | * | 929 | 773 | 577 | 382 |
| 14 | 1170 | F _v | 1147 | 762 | 633 | 473 | 312 |
| 15 | 1091 | F _v | 951 | 631 | 524 | 391 | 258 |
| 16 | 1022 | F _v | 796 | 528 | 438 | 327 | 215 |
| 17 | 962 | F _v | 673 | 445 | 370 | 275 | 180 |
| 18 | 862 | F _b | 573 | 379 | 314 | 233 | 153 |
| 19 | 773 | F _b | 491 | 324 | 269 | 199 | 130 |
| 20 | 696 | F _b | 424 | 279 | 231 | 171 | 111 |
| 21 | 631 | F _b | 368 | 242 | 200 | 148 | 96 |
| 22 | 574 | F _b | 321 | 211 | 174 | 129 | 83 |
| 23 | 524 | F _b | 282 | 185 | 152 | 112 | 72 |
| 24 | 481 | F _b | 248 | 162 | 134 | 98 | 62 |
| 25 | 442 | F _b | 220 | 143 | 118 | 86 | 55 |
| 26 | 408 | F _b | 195 | 127 | 104 | 76 | 48 |
| 27 | 378 | F _b | 174 | 113 | 93 | 67 | 42 |
| 28 | 351 | F _b | 156 | 101 | 83 | 60 | 37 |
| 29 | 327 | F _b | 140 | 90 | 74 | 53 | 32 |
| 30 | 305 | F _b | 126 | 81 | 66 | 47 | 28 |

The part weight has been deduced in the above table

18 X 3/8 X 4 1/2 X 1/2 I-BEAM
 $A_w=6.375 \text{ in}^2$ $I_x=498.15 \text{ in}^4$ $S_x=55.35 \text{ in}^3$ $Wt.=8.70 \text{ lbs./ft}$

| SPAN FEET | MAXIMUM LOAD | | DEFLECTION | | | | |
|-----------|--------------|----------------|------------|-------|-------|-------|-------|
| | | | L/100 | L/150 | L/180 | L/240 | L/360 |
| 8 | 2382 | F _v | * | * | * | * | 1996 |
| 9 | 2116 | F _v | * | * | * | * | 1565 |
| 10 | 1904 | F _v | * | * | * | 1872 | 1245 |
| 11 | 1730 | F _v | * | * | * | 1507 | 1002 |
| 12 | 1585 | F _v | * | * | * | 1228 | 816 |
| 13 | 1462 | F _v | * | * | 1351 | 1011 | 671 |
| 14 | 1357 | F _v | * | 1349 | 1123 | 840 | 557 |
| 15 | 1266 | F _v | * | 1132 | 942 | 704 | 466 |
| 16 | 1186 | F _v | * | 957 | 796 | 595 | 394 |
| 17 | 1116 | F _v | * | 815 | 678 | 506 | 335 |
| 18 | 1054 | F _v | * | 700 | 581 | 434 | 286 |
| 19 | 998 | F _v | 910 | 604 | 502 | 374 | 246 |
| 20 | 913 | F _b | 791 | 524 | 436 | 324 | 213 |
| 21 | 828 | F _b | 691 | 458 | 380 | 283 | 186 |
| 22 | 753 | F _b | 607 | 402 | 333 | 248 | 162 |
| 23 | 688 | F _b | 536 | 354 | 294 | 218 | 142 |
| 24 | 632 | F _b | 475 | 313 | 260 | 193 | 125 |
| 25 | 581 | F _b | 422 | 279 | 231 | 171 | 111 |
| 26 | 537 | F _b | 377 | 248 | 206 | 152 | 98 |
| 27 | 497 | F _b | 338 | 222 | 184 | 136 | 87 |
| 28 | 462 | F _b | 304 | 200 | 165 | 121 | 78 |
| 29 | 430 | F _b | 274 | 180 | 148 | 109 | 70 |
| 30 | 401 | F _b | 248 | 162 | 134 | 98 | 62 |

The part weight has been deduced in the above table

24 X 3/8 X 7 1/2 X 3/4 I-BEAM
 $A_w=8.44 \text{ in}^2$ $I_x=1877 \text{ in}^4$ $S_x=156.42 \text{ in}^3$ $Wt.=15.20 \text{ lbs./ft}$

| SPAN FEET | MAXIMUM LOAD | | DEFLECTION | | | | |
|-----------|--------------|----------------|------------|-------|-------|-------|-------|
| | | | L/100 | L/150 | L/180 | L/240 | L/360 |
| 35 | 707 | F _v | 552 | 363 | 300 | 221 | 142 |
| 36 | 687 | F _v | 510 | 335 | 276 | 203 | 130 |
| 37 | 668 | F _v | 472 | 309 | 255 | 187 | 119 |
| 38 | 650 | F _v | 437 | 286 | 236 | 173 | 110 |
| 39 | 633 | F _v | 405 | 265 | 218 | 160 | 101 |
| 40 | 617 | F _v | 377 | 246 | 202 | 148 | 93 |
| 41 | 602 | F _v | 350 | 228 | 188 | 137 | 86 |
| 42 | 575 | F _b | 327 | 212 | 174 | 127 | 79 |
| 43 | 548 | F _b | 305 | 198 | 162 | 118 | 73 |
| 44 | 523 | F _b | 284 | 184 | 151 | 109 | 67 |
| 45 | 499 | F _b | 266 | 172 | 141 | 101 | 62 |
| 46 | 477 | F _b | 249 | 161 | 131 | 94 | 58 |
| 47 | 456 | F _b | 233 | 150 | 122 | 88 | 53 |
| 48 | 437 | F _b | 219 | 140 | 114 | 82 | 49 |
| 49 | 418 | F _b | 205 | 131 | 107 | 76 | 45 |
| 50 | 401 | F _b | 193 | 123 | 100 | 71 | 42 |
| 51 | 385 | F _b | 181 | 116 | 94 | 66 | 39 |
| 52 | 370 | F _b | 171 | 108 | 88 | 62 | 36 |
| 53 | 355 | F _b | 161 | 102 | 82 | 58 | 33 |
| 54 | 342 | F _b | 151 | 96 | 77 | 54 | 31 |
| 55 | 329 | F _b | 143 | 90 | 72 | 50 | 28 |
| 56 | 316 | F _b | 135 | 84 | 68 | 47 | 26 |
| 57 | 305 | F _b | 127 | 79 | 64 | 44 | 24 |

The part weight has been deduced in the above table

3 X 13/16 X 1/8 CHANNEL
 $A_w=0.344 \text{ in}^2$ $I_x=0.64 \text{ in}^4$ $S_x=0.43 \text{ in}^3$ $Wt.=0.43 \text{ lbs./ft}$

| SPAN FEET | MAXIMUM LOAD | | DEFLECTION | | | | |
|-----------|--------------|----------------|------------|-------|-------|-------|-------|
| | | | L/100 | L/150 | L/180 | L/240 | L/360 |
| 3 | 317 | F _b | 301 | 200 | 167 | 125 | 83 |
| 4 | 178 | F _b | 135 | 90 | 75 | 56 | 37 |
| 5 | 114 | F _b | 71 | 47 | 39 | 29 | 19 |
| 6 | 79 | F _b | 41 | 27 | 23 | 17 | 11 |
| 7 | 57 | F _b | 26 | 17 | 14 | 10 | 7 |
| 8 | 44 | F _b | 17 | 11 | 9 | 7 | 4 |
| 9 | 34 | F _b | 12 | 8 | 6 | 4 | 3 |
| 10 | 28 | F _b | 8 | 5 | 4 | 3 | 2 |

The part weight has been deduced in the above table

3 X 1 X 1/4 CHANNEL
 $A_w=0.625 \text{ in}^2$ $I_x=1.27 \text{ in}^4$ $S_x=0.85 \text{ in}^3$ $Wt.=0.85 \text{ lbs./ft}$

| SPAN FEET | MAXIMUM LOAD | | DEFLECTION | | | | |
|-----------|--------------|----------------|------------|-------|-------|-------|-------|
| | | | L/100 | L/150 | L/180 | L/240 | L/360 |
| 3 | 624 | F _v | 591 | 393 | 328 | 246 | 163 |
| 4 | 353 | F _b | 267 | 178 | 148 | 111 | 73 |
| 5 | 226 | F _b | 141 | 94 | 78 | 58 | 38 |
| 6 | 156 | F _b | 83 | 55 | 46 | 34 | 22 |
| 7 | 115 | F _b | 52 | 35 | 29 | 21 | 14 |
| 8 | 88 | F _b | 35 | 23 | 19 | 14 | 9 |
| 9 | 69 | F _b | 24 | 16 | 13 | 10 | 6 |
| 10 | 56 | F _b | 18 | 11 | 9 | 7 | 4 |

The part weight has been deduced in the above table

3 X 1 1/2 X 1/4 CHANNEL
 $A_w=0.625 \text{ in}^2$ $I_x=1.75 \text{ in}^4$ $S_x=1.16 \text{ in}^3$ $Wt.=1.01 \text{ lbs./ft}$

| SPAN FEET | MAXIMUM LOAD | | DEFLECTION | | | | |
|-----------|--------------|----------------|------------|-------|-------|-------|-------|
| | | | L/100 | L/150 | L/180 | L/240 | L/360 |
| 3 | 623 | F _v | * | 511 | 425 | 319 | 212 |
| 4 | 467 | F _v | 355 | 236 | 196 | 147 | 97 |
| 5 | 307 | F _b | 189 | 126 | 104 | 78 | 51 |
| 6 | 213 | F _b | 112 | 74 | 61 | 45 | 30 |
| 7 | 156 | F _b | 71 | 46 | 38 | 28 | 18 |
| 8 | 119 | F _b | 47 | 31 | 25 | 19 | 12 |
| 9 | 93 | F _b | 33 | 21 | 17 | 13 | 8 |
| 10 | 75 | F _b | 24 | 15 | 12 | 9 | 5 |

The part weight has been deduced in the above table

3 1/2 X 1 3/16 X 1/8 X 3/16 CHANNEL
 $A_w=0.406 \text{ in}^2$ $I_x=1.54 \text{ in}^4$ $S_x=0.88 \text{ in}^3$ $Wt.=0.67 \text{ lbs./ft}$

| SPAN FEET | MAXIMUM LOAD | | DEFLECTION | | | | |
|-----------|--------------|----------------|------------|-------|-------|-------|-------|
| | | | L/100 | L/150 | L/180 | L/240 | L/360 |
| 3 | 623 | F _v | * | 511 | 425 | 319 | 212 |
| 4 | 467 | F _v | 355 | 236 | 196 | 147 | 97 |
| 5 | 307 | F _b | 189 | 126 | 104 | 78 | 51 |
| 6 | 213 | F _b | 112 | 74 | 61 | 45 | 30 |
| 7 | 156 | F _b | 71 | 46 | 38 | 28 | 18 |
| 8 | 119 | F _b | 47 | 31 | 25 | 19 | 12 |
| 9 | 93 | F _b | 33 | 21 | 17 | 13 | 8 |
| 10 | 75 | F _b | 24 | 15 | 12 | 9 | 5 |

The part weight has been deduced in the above table

4 X 1 3/8 X 3/16 CHANNEL
 $A_w=0.680 \text{ in}^2$ $I_x=2.62 \text{ in}^4$ $S_x=1.31 \text{ in}^3$ $Wt.=0.88 \text{ lbs./ft}$

| SPAN FEET | MAXIMUM LOAD | | DEFLECTION | | | | |
|-----------|--------------|-------|------------|-------|-------|-------|-------|
| | | | L/100 | L/150 | L/180 | L/240 | L/360 |
| 3 | 679 | F_v | * | * | 593 | 445 | 296 |
| 4 | 509 | F_v | 509 | 339 | 282 | 211 | 141 |
| 5 | 348 | F_b | 277 | 184 | 153 | 115 | 76 |
| 6 | 242 | F_b | 165 | 110 | 91 | 68 | 45 |
| 7 | 177 | F_b | 106 | 70 | 58 | 44 | 29 |
| 8 | 135 | F_b | 72 | 48 | 39 | 29 | 19 |
| 9 | 107 | F_b | 51 | 33 | 28 | 21 | 13 |
| 10 | 86 | F_b | 37 | 24 | 20 | 15 | 10 |

The part weight has been deduced in the above table

4 X 1 1/8 X 1/4 CHANNEL
 $A_w=0.875 \text{ in}^2$ $I_x=2.87 \text{ in}^4$ $S_x=1.44 \text{ in}^3$ $Wt.=1.05 \text{ lbs./ft}$

| SPAN FEET | MAXIMUM LOAD | | DEFLECTION | | | | |
|-----------|--------------|-------|------------|-------|-------|-------|-------|
| | | | L/100 | L/150 | L/180 | L/240 | L/360 |
| 3 | 873 | F_v | * | 811 | 675 | 506 | 337 |
| 4 | 598 | F_b | 570 | 380 | 316 | 236 | 157 |
| 5 | 382 | F_b | 307 | 204 | 170 | 127 | 84 |
| 6 | 265 | F_b | 182 | 121 | 100 | 75 | 49 |
| 7 | 194 | F_b | 116 | 77 | 64 | 47 | 31 |
| 8 | 148 | F_b | 78 | 52 | 43 | 31 | 20 |
| 9 | 117 | F_b | 55 | 36 | 30 | 22 | 14 |
| 10 | 94 | F_b | 40 | 26 | 21 | 15 | 10 |

The part weight has been deduced in the above table

6 X 1 5/8 X 1/4 CHANNEL
 $A_w=1.375 \text{ in}^2$ $I_x=10.18 \text{ in}^4$ $S_x=3.39 \text{ in}^3$ $Wt.=1.67 \text{ lbs./ft}$

| SPAN FEET | MAXIMUM LOAD | | DEFLECTION | | | | |
|-----------|--------------|-------|------------|-------|-------|-------|-------|
| | | | L/100 | L/150 | L/180 | L/240 | L/360 |
| 5 | 823 | F_v | * | 649 | 540 | 405 | 269 |
| 6 | 626 | F_b | 599 | 399 | 332 | 249 | 165 |
| 7 | 459 | F_b | 392 | 261 | 217 | 162 | 107 |
| 8 | 351 | F_b | 269 | 179 | 149 | 111 | 73 |
| 9 | 277 | F_b | 192 | 127 | 106 | 79 | 52 |
| 10 | 224 | F_b | 141 | 93 | 78 | 58 | 38 |
| 11 | 185 | F_b | 107 | 70 | 58 | 43 | 28 |
| 12 | 155 | F_b | 82 | 54 | 45 | 33 | 21 |
| 13 | 132 | F_b | 65 | 43 | 35 | 26 | 17 |
| 14 | 113 | F_b | 52 | 34 | 28 | 20 | 13 |
| 15 | 98 | F_b | 42 | 27 | 22 | 16 | 10 |

The part weight has been deduced in the above table

6 X 1 11/16 X 3/8 CHANNEL
 $A_w=1.969 \text{ in}^2$ $I_x=14.55 \text{ in}^4$ $S_x=4.86 \text{ in}^3$ $Wt.=2.39 \text{ lbs./ft}$

| SPAN FEET | MAXIMUM LOAD | | DEFLECTION | | | | |
|-----------|--------------|-------|------------|-------|-------|-------|-------|
| | | | L/100 | L/150 | L/180 | L/240 | L/360 |
| 5 | 1178 | F_v | * | 928 | 773 | 579 | 385 |
| 6 | 895 | F_b | 857 | 570 | 475 | 355 | 236 |
| 7 | 657 | F_b | 560 | 372 | 310 | 232 | 153 |
| 8 | 502 | F_b | 384 | 255 | 212 | 158 | 105 |
| 9 | 396 | F_b | 274 | 182 | 151 | 112 | 74 |
| 10 | 320 | F_b | 202 | 133 | 111 | 82 | 54 |
| 11 | 264 | F_b | 152 | 101 | 83 | 62 | 40 |
| 12 | 222 | F_b | 118 | 77 | 64 | 47 | 31 |
| 13 | 188 | F_b | 92 | 61 | 50 | 37 | 24 |
| 14 | 162 | F_b | 74 | 48 | 40 | 29 | 18 |
| 15 | 141 | F_b | 60 | 39 | 32 | 23 | 14 |

The part weight has been deduced in the above table

8 X 2-3/16 X 3/8 CHANNEL
 $A_w=2.719 \text{ in}^2$ $I_x=35.77 \text{ in}^4$ $S_x=8.94 \text{ in}^3$ $Wt.=3.20 \text{ lbs./ft}$

| SPAN FEET | MAXIMUM LOAD | | DEFLECTION | | | | |
|-----------|--------------|-------|------------|-------|-------|-------|-------|
| | | | L/100 | L/150 | L/180 | L/240 | L/360 |
| 5 | 1627 | F_v | * | * | * | 1235 | 822 |
| 6 | 1356 | F_v | * | 1261 | 1050 | 787 | 523 |
| 7 | 1161 | F_v | * | 845 | 704 | 527 | 350 |
| 8 | 927 | F_b | 887 | 590 | 491 | 367 | 244 |
| 9 | 732 | F_b | 642 | 426 | 355 | 265 | 175 |
| 10 | 592 | F_b | 478 | 317 | 264 | 197 | 130 |
| 11 | 489 | F_b | 364 | 241 | 201 | 149 | 98 |
| 12 | 410 | F_b | 283 | 188 | 156 | 116 | 76 |
| 13 | 349 | F_b | 224 | 148 | 123 | 91 | 59 |
| 14 | 300 | F_b | 180 | 119 | 98 | 73 | 47 |
| 15 | 261 | F_b | 147 | 97 | 80 | 59 | 38 |
| 16 | 229 | F_b | 121 | 79 | 65 | 48 | 31 |
| 17 | 202 | F_b | 101 | 66 | 54 | 40 | 25 |
| 18 | 180 | F_b | 85 | 55 | 45 | 33 | 21 |
| 19 | 161 | F_b | 72 | 46 | 38 | 27 | 17 |
| 20 | 145 | F_b | 61 | 39 | 32 | 23 | 14 |

The part weight has been deduced in the above table

10 X 2-3/4 X 1/2 CHANNEL
 $A_w=4.500 \text{ in}^2$ $I_x=92.49 \text{ in}^4$ $S_x=18.50 \text{ in}^3$ $Wt.=5.30 \text{ lbs./ft}$

| SPAN FEET | MAXIMUM LOAD | | DEFLECTION | | | | |
|--------------|--------------|----------------|------------|-------|-------|-------|-------|
| | | | L/100 | L/150 | L/180 | L/240 | L/360 |
| 6 | 2244 | F _v | * | * | * | 1802 | 1199 |
| 7 | 1923 | F _v | * | * | 1654 | 1239 | 824 |
| 8 | 1682 | F _v | * | 1414 | 1177 | 882 | 586 |
| 9 | 1494 | F _v | * | 1037 | 864 | 646 | 429 |
| 10 | 1227 | F _b | 1174 | 781 | 650 | 486 | 322 |
| 11 | 1013 | F _b | 904 | 600 | 499 | 373 | 247 |
| 12 | 850 | F _b | 709 | 470 | 391 | 292 | 193 |
| 13 | 724 | F _b | 565 | 375 | 311 | 232 | 153 |
| 14 | 623 | F _b | 457 | 303 | 251 | 187 | 123 |
| 15 | 542 | F _b | 374 | 248 | 205 | 153 | 100 |
| 16 | 476 | F _b | 310 | 205 | 170 | 126 | 82 |
| 17 | 421 | F _b | 259 | 171 | 141 | 105 | 68 |
| 18 | 375 | F _b | 219 | 144 | 119 | 88 | 56 |
| 19 | 336 | F _b | 186 | 122 | 101 | 74 | 47 |
| 20 | 302 | F _b | 160 | 104 | 86 | 63 | 40 |
| 21 | 274 | F _b | 138 | 90 | 74 | 54 | 34 |
| 22 | 249 | F _b | 119 | 78 | 64 | 46 | 29 |
| 23 | 227 | F _b | 104 | 67 | 55 | 40 | 25 |
| 24 | 208 | F _b | 91 | 59 | 48 | 34 | 21 |
| 25 | 191 | F _b | 80 | 51 | 42 | 30 | 18 |

The part weight has been deduced in the above table

3 X 1/4 SQUARE TUBE
 $A_w=1.250 \text{ in}^2$ $I_x=3.50 \text{ in}^4$ $S_x=2.33 \text{ in}^3$ $Wt.=2.07 \text{ lbs./ft}$

| SPAN FEET | MAXIMUM LOAD | | DEFLECTION | | | | |
|--------------|--------------|----------------|------------|-------|-------|-------|-------|
| | | | L/100 | L/150 | L/180 | L/240 | L/360 |
| 4 | 935 | F _v | 710 | 472 | 393 | 294 | 195 |
| 5 | 618 | F _b | 380 | 252 | 210 | 156 | 103 |
| 6 | 428 | F _b | 224 | 149 | 123 | 92 | 60 |
| 7 | 314 | F _b | 142 | 94 | 78 | 58 | 37 |
| 8 | 240 | F _b | 96 | 63 | 52 | 38 | 24 |
| 9 | 189 | F _b | 67 | 43 | 36 | 26 | 16 |
| 10 | 152 | F _b | 48 | 31 | 25 | 18 | 11 |
| 11 | 125 | F _b | 36 | 23 | 18 | 13 | 8 |
| 12 | 105 | F _b | 27 | 17 | 14 | 9 | 5 |

The part weight has been deduced in the above table

4 X 1/4 SQUARE TUBE
 $A_w=1.750 \text{ in}^2$ $I_x=8.82 \text{ in}^4$ $S_x=4.41 \text{ in}^3$ $Wt.=2.83 \text{ lbs./ft}$

| SPAN FEET | MAXIMUM LOAD | | DEFLECTION | | | | |
|--------------|--------------|-------|------------|-------|-------|-------|-------|
| | | | L/100 | L/150 | L/180 | L/240 | L/360 |
| 4 | 1310 | F_v | * | 1085 | 903 | 677 | 450 |
| 5 | 1047 | F_v | 900 | 599 | 499 | 373 | 248 |
| 6 | 814 | F_b | 543 | 361 | 301 | 225 | 149 |
| 7 | 597 | F_b | 351 | 233 | 194 | 144 | 95 |
| 8 | 456 | F_b | 238 | 158 | 131 | 98 | 64 |
| 9 | 360 | F_b | 169 | 112 | 92 | 69 | 45 |
| 10 | 291 | F_b | 123 | 81 | 67 | 50 | 32 |
| 11 | 240 | F_b | 93 | 61 | 50 | 37 | 24 |
| 12 | 201 | F_b | 71 | 46 | 38 | 28 | 18 |
| 13 | 171 | F_b | 56 | 36 | 30 | 21 | 13 |
| 14 | 147 | F_b | 44 | 28 | 23 | 17 | 10 |
| 15 | 128 | F_b | 35 | 23 | 18 | 13 | 8 |

The part weight has been deduced in the above table

Introduction To Columns and Column tables

COLUMNS

Full section column testing was conducted on equal leg angles, I-Beams, Wide Flange Beams and Square Tubes. Ultimate values were generated through testing of elements with square cut ends placed between the table and the upper, moving platen of a universal testing machine. This test procedure closely simulates how FRP columns will generally be used in practice. Comparison of test data versus theoretical Euler buckling capacity suggests that the "K" value as tested is approximately 0.70, representing a fixed-pinned condition. The values in the tables represent a FS=3.0 for the tested condition. Should you feel, however, that your column end conditions closely approximate a pinned-pinned condition ("rounded" column ends are somewhat difficult to achieve in practice) we recommend you multiply the allowable values shown by the following values:

| SHAPE | To Obtain FS=2.0 multiply by: | To Obtain FS=3.0 multiply by: |
|---------------|----------------------------------|----------------------------------|
| I, W or Angle | 0.75 | 0.50 |
| Square Tube | 0.50 | 0.33 |

COLUMN TABLES

- A - area (in²)
- b - width of flange/leg/wall (in)
- t - thickness of flange (in)
- r - minimum radius gyration (in)
- l - length (in)
- K - effective column length factor
- F_a - allowable column concentric axial stress (psi)
- P_a - allowable column concentric axial stress (lbs)

Angle

Maximum allowable stress:

| | |
|------------|-----------|
| b/t ! 8 | 4,862 psi |
| b/t = 10.7 | 4,194 psi |
| b/t = 12 | 3,620 psi |
| b/t = 16 | 2,758 psi |

Square tube (1/4" wall)

Maximum allowable stress:

| | |
|----------|------------|
| b/t ! 10 | 10,000 psi |
| b/t = 12 | 8,880 psi |
| b/t = 16 | 6,595 psi |

Wide-Flange & I-Beam

Maximum allowable stress:

| | | |
|----------|------------|------------|
| | b/t ! 12 | 10,000 psi |
| | b/t = 13.3 | 8,747 psi |
| t = 1/4" | b/t = 16 | 7,208 psi |
| t > 1/4" | b/t = 16 | 6,233 psi |
| | b/t = 20 | 4,920 psi |
| | b/t = 21.3 | 4,483 psi |
| t = 1/4" | b/t = 24 | 4,167 psi |
| t > 1/4" | b/t = 24 | 3,608 psi |
| | b/t = 26.7 | 2,732 psi |

Column Tables
Allowable Concentric Axial Stresses and Loads

2 X 2 X 1/4 ANGLE

A = 0.92 in²
r = 0.38 in
b/t = 8

| TRUE LENGTH (ft) | F _a (psi) | P _a (lbs) |
|------------------|----------------------|----------------------|
| 0.5 | 4.862 | 4.473 |
| 1.0 | 2.807 | 2.582 |
| 1.5 | 2.077 | 1.911 |
| 2.0 | 1.684 | 1.549 |
| 2.5 | 1.416 | 1.303 |
| 3.0 | 1.211 | 1.114 |
| 3.5 | 1.079 | 993 |
| 4.0 | 988 | 909 |
| 4.5 | 891 | 820 |
| 5.0 | 833 | 766 |
| 5.5 | 752 | 692 |
| 6.0 | 667 | 614 |

The effective 'K' value is 0.70. 'K' equals effective column length factor. See introduction to column tables showing notation factors

3 X 3 X 1/4 ANGLE

A = 1.42 in²
r = 0.9 in
b/t = 12

| TRUE LENGTH (ft) | F _a (psi) | P _a (lbs) |
|------------------|----------------------|----------------------|
| 0.5 | 3.620 | 5.140 |
| 1.0 | 3.620 | 5.140 |
| 1.5 | 2.933 | 4.165 |
| 2.0 | 2.277 | 3.233 |
| 2.5 | 1.968 | 2.795 |
| 3.0 | 1.736 | 2.465 |
| 3.5 | 1.538 | 2.184 |
| 4.0 | 1.391 | 1.975 |
| 4.5 | 1.249 | 1.774 |
| 5.0 | 1.146 | 1.627 |
| 5.5 | 1.070 | 1.519 |
| 6.0 | 1.010 | 1.434 |
| 6.5 | 952 | 1.352 |
| 7.0 | 889 | 1.262 |
| 7.5 | 849 | 1.206 |
| 8.0 | 815 | 1.157 |
| 8.5 | 757 | 1.075 |
| 9.0 | 708 | 1.005 |
| 9.5 | 665 | 944 |

The effective 'K' value is 0.70. 'K' equals effective column length factor. See introduction to column tables showing notation factors

3 X 3 X 3/8 ANGLE

$A = 2.09 \text{ in}^2$

$r = 0.59 \text{ in}$

$b/t = 8$

| TRUE LENGTH (ft) | F_a (psi) | P_a (lbs) |
|------------------|-------------|-------------|
| 0.5 | 4.862 | 10.162 |
| 1.0 | 4.862 | 10.162 |
| 1.5 | 2.933 | 6.130 |
| 2.0 | 2.277 | 4.756 |
| 2.5 | 1.968 | 4.113 |
| 3.0 | 1.736 | 3.628 |
| 3.5 | 1.538 | 3.214 |
| 4.0 | 1.391 | 2.907 |
| 4.5 | 1.249 | 2.610 |
| 5.0 | 1.146 | 2.395 |
| 5.5 | 1.070 | 2.236 |
| 6.0 | 1.010 | 2.111 |
| 6.5 | 952 | 1.990 |
| 7.0 | 889 | 1.858 |
| 7.5 | 849 | 1.774 |
| 8.0 | 815 | 1.703 |
| 8.5 | 757 | 1.582 |
| 9.0 | 708 | 1.480 |
| 9.5 | 665 | 1.390 |

The effective 'K' value is 0.70. 'K' equals effective column length factor. See introduction to column tables showing notation factors

3 X 3 X 1/2 ANGLE

$A = 2.70 \text{ in}^2$

$r = 0.59 \text{ in}$

$b/t = 6$

| TRUE LENGTH (ft) | F_a (psi) | P_a (lbs) |
|------------------|-------------|-------------|
| 0.5 | 4.862 | 13.127 |
| 1.0 | 4.862 | 13.127 |
| 1.5 | 2.933 | 7.919 |
| 2.0 | 2.277 | 6.148 |
| 2.5 | 1.968 | 5.314 |
| 3.0 | 1.736 | 4.687 |
| 3.5 | 1.538 | 4.153 |
| 4.0 | 1.391 | 3.756 |
| 4.5 | 1.249 | 3.372 |
| 5.0 | 1.146 | 3.094 |
| 5.5 | 1.070 | 2.889 |
| 6.0 | 1.010 | 2.727 |
| 6.5 | 952 | 2.570 |
| 7.0 | 889 | 2.400 |
| 7.5 | 849 | 2.292 |
| 8.0 | 815 | 2.201 |
| 8.5 | 757 | 2.044 |
| 9.0 | 708 | 1.912 |
| 9.5 | 665 | 1.796 |

The effective 'K' value is 0.70. 'K' equals effective column length factor. See introduction to column tables showing notation factors

4 X 4 X 1/4 ANGLE

$A = 1.92 \text{ in}^2$

$r = 0.80 \text{ in}$

$b/t = 16$

| TRUE LENGTH (ft) | F_a (psi) | P_a (lbs) |
|------------------|-------------|-------------|
| 0.5 | 2,758 | 5,295 |

| | | |
|------|-------|-------|
| 1.0 | 2.758 | 5.295 |
| 1.5 | 2.758 | 5.295 |
| 2.0 | 2.758 | 5.295 |
| 2.5 | 2.393 | 4.595 |
| 3.0 | 2.133 | 4.095 |
| 3.5 | 1.914 | 3.675 |
| 4.0 | 1.760 | 3.379 |
| 4.5 | 1.603 | 3.078 |
| 5.0 | 1.482 | 2.845 |
| 5.5 | 1.379 | 2.648 |
| 6.0 | 1.283 | 2.463 |
| 6.5 | 1.187 | 2.279 |
| 7.0 | 1.123 | 2.156 |
| 7.5 | 1.064 | 2.043 |
| 8.0 | 1.020 | 1.958 |
| 8.5 | 980 | 1.882 |
| 9.0 | 933 | 1.791 |
| 9.5 | 889 | 1.707 |
| 10.0 | 860 | 1.651 |
| 10.5 | 834 | 1.601 |
| 11.0 | 802 | 1.540 |
| 11.5 | 759 | 1.457 |
| 12.0 | 727 | 1.396 |
| 12.5 | 693 | 1.331 |
| 13.0 | 660 | 1.267 |

The effective 'K' value is 0.70. 'K' equals effective column length factor. See introduction to column tables showing notation factors

4 X 4 X 3/8 ANGLE

$A = 2.84 \text{ in}^2$

$r = 0.79 \text{ in}$

$b/t = 10.7$

| TRUE LENGTH (ft) | F_a (psi) | P_a (lbs) |
|---------------------|----------------|----------------|
| 0.5 | 4,194 | 11,911 |
| 1.0 | 4,194 | 11,911 |
| 1.5 | 4,194 | 11,911 |
| 2.0 | 2,947 | 8,369 |
| 2.5 | 2,367 | 6,722 |
| 3.0 | 2,113 | 6,001 |
| 3.5 | 1,896 | 5,385 |
| 4.0 | 1,741 | 4,944 |
| 4.5 | 1,586 | 4,504 |
| 5.0 | 1,461 | 4,149 |
| 5.5 | 1,364 | 3,874 |
| 6.0 | 1,260 | 3,578 |
| 6.5 | 1,177 | 3,343 |
| 7.0 | 1,113 | 3,161 |
| 7.5 | 1,048 | 2,976 |
| 8.0 | 1,012 | 2,874 |
| 8.5 | 969 | 2,752 |
| 9.0 | 922 | 2,618 |
| 9.5 | 878 | 2,494 |
| 10.0 | 853 | 2,423 |
| 10.5 | 828 | 2,352 |
| 11.0 | 791 | 2,246 |
| 11.5 | 745 | 2,116 |
| 12.0 | 712 | 2,022 |
| 12.5 | 680 | 1,931 |
| 13.0 | 652 | 1,852 |

The effective 'K' value is 0.70. 'K' equals effective column length factor. See introduction to column tables showing notation factors

6 X 6 X 3/8 ANGLE

$A = 4.33 \text{ in}^2$

$r = 1.14 \text{ in}$

$b/t = 16$

| TRUE LENGTH (ft) | F_a (psi) | P_a (lbs) |
|---------------------|----------------|----------------|
| 0.5 | 2.758 | 11.942 |
| 1.0 | 2.758 | 11.942 |
| 1.5 | 2.758 | 11.942 |
| 2.0 | 2.758 | 11.942 |
| 2.5 | 2.758 | 11.942 |
| 3.0 | 2.758 | 11.942 |
| 3.5 | 2.427 | 10.509 |
| 4.0 | 2.229 | 9.652 |
| 4.5 | 2.060 | 8.920 |
| 5.0 | 1.911 | 8.275 |
| 5.5 | 1.802 | 7.803 |
| 6.0 | 1.684 | 7.292 |
| 6.5 | 1.585 | 6.863 |
| 7.0 | 1.503 | 6.508 |
| 7.5 | 1.416 | 6.131 |
| 8.0 | 1.354 | 5.863 |
| 8.5 | 1.289 | 5.581 |
| 9.0 | 1.211 | 5.244 |
| 9.5 | 1.167 | 5.053 |
| 10.0 | 1.121 | 4.854 |
| 10.5 | 1.079 | 4.672 |
| 11.0 | 1.041 | 4.508 |
| 11.5 | 1.015 | 4.395 |
| 12.0 | 988 | 4.278 |
| 12.5 | 955 | 4.135 |
| 13.0 | 922 | 3.992 |
| 13.5 | 892 | 3.862 |
| 14.0 | 872 | 3.776 |
| 14.5 | 851 | 3.685 |
| 15.0 | 833 | 3.607 |
| 15.5 | 813 | 3.520 |
| 16.0 | 782 | 3.386 |
| 16.5 | 752 | 3.256 |
| 17.0 | 729 | 3.157 |
| 17.5 | 706 | 3.057 |
| 18.0 | 680 | 2.944 |
| 18.5 | 660 | 2.858 |

The effective 'K' value is 0.70. 'K' equals effective column length factor. See introduction to column tables showing notation factors

6 X 6 X 1/2 ANGLE

$A = 5.70 \text{ in}^2$

$r = 1.19 \text{ in}$

$b/t = 12$

| TRUE LENGTH (ft) | F_a (psi) | P_a (lbs) |
|---------------------|----------------|----------------|
| 0.5 | 3.620 | 20.634 |
| 1.0 | 3.620 | 20.634 |
| 1.5 | 3.620 | 20.634 |
| 2.0 | 3.620 | 20.634 |
| 2.5 | 3.620 | 20.634 |
| 3.0 | 2.960 | 16.872 |
| 3.5 | 2.512 | 14.318 |
| 4.0 | 2.290 | 13.053 |
| 4.5 | 2.120 | 12.084 |
| 5.0 | 1.984 | 11.309 |
| 5.5 | 1.844 | 10.511 |
| 6.0 | 1.748 | 9.964 |
| 6.5 | 1.642 | 9.359 |
| 7.0 | 1.548 | 8.824 |
| 7.5 | 1.469 | 8.373 |
| 8.0 | 1.397 | 7.963 |
| 8.5 | 1.337 | 7.621 |
| 9.0 | 1.267 | 7.222 |
| 9.5 | 1.202 | 6.851 |
| 10.0 | 1.157 | 6.595 |
| 10.5 | 1.117 | 6.367 |
| 11.0 | 1.076 | 6.133 |
| 11.5 | 1.033 | 5.888 |
| 12.0 | 1.015 | 5.786 |
| 12.5 | 989 | 5.637 |
| 13.0 | 958 | 5.461 |
| 13.5 | 927 | 5.284 |
| 14.0 | 896 | 5.107 |
| 14.5 | 873 | 4.976 |
| 15.0 | 855 | 4.874 |
| 15.5 | 839 | 4.782 |
| 16.0 | 822 | 4.685 |
| 16.5 | 794 | 4.526 |
| 17.0 | 765 | 4.361 |
| 17.5 | 737 | 4.201 |
| 18.0 | 717 | 4.087 |
| 18.5 | 699 | 3.984 |
| 19.0 | 672 | 3.830 |
| 19.5 | 655 | 3.734 |

The effective 'K' value is 0.70. 'K' equals effective column length factor. See introduction to column tables showing notation factors

3 X 1-1/2 X 1/4 I-BEAM

$$A = 1.38 \text{ in}^2$$

$$r = 0.32 \text{ in}$$

$$b/t = 6$$

| TRUE LENGTH (ft) | F _a (psi) | P _a (lbs) |
|------------------|----------------------|----------------------|
| 0.5 | 10.000 | 13.800 |
| 1.0 | 8.121 | 11.207 |
| 1.5 | 5.155 | 7.114 |
| 2.0 | 3.583 | 4.945 |
| 2.5 | 2.462 | 3.398 |
| 3.0 | 1.683 | 2.323 |
| 3.5 | 1.278 | 1.764 |
| 4.0 | 1.027 | 1.417 |
| 4.5 | 843 | 1.163 |
| 5.0 | 652 | 900 |

The effective 'K' value is 0.70. 'K' equals effective column length factor. See introduction to column tables showing notation factors

4 X 2 X 1/4 I-BEAM

$$A = 1.88 \text{ in}^2$$

$$r = 0.43 \text{ in}$$

$$b/t = 8$$

| TRUE LENGTH (ft) | F _a (psi) | P _a (lbs) |
|------------------|----------------------|----------------------|
| 0.5 | 10.000 | 18.800 |
| 1.0 | 10.000 | 18.800 |
| 1.5 | 7.107 | 13.361 |
| 2.0 | 5.206 | 9.787 |
| 2.5 | 4.061 | 7.635 |
| 3.0 | 3.017 | 5.672 |
| 3.5 | 2.248 | 4.226 |
| 4.0 | 1.717 | 3.228 |
| 4.5 | 1.373 | 2.581 |
| 5.0 | 1.147 | 2.156 |
| 5.5 | 992 | 1.865 |
| 6.0 | 854 | 1.606 |
| 6.5 | 713 | 1.340 |
| 7.0 | 567 | 1.066 |

The effective 'K' value is 0.70. 'K' equals effective column length factor. See introduction to column tables showing notation factors

6 X 3 X 1/4 I-BEAM

$A = 2.88 \text{ in}^2$

$r = 0.63 \text{ in}$

$b/t = 12$

| TRUE LENGTH (ft) | F_a (psi) | P_a (lbs) |
|---------------------|----------------|----------------|
| 0.5 | 10.000 | 28.800 |
| 1.0 | 10.000 | 28.800 |
| 1.5 | 10.000 | 28.800 |
| 2.0 | 7.944 | 22.879 |
| 2.5 | 6.127 | 17.646 |
| 3.0 | 5.083 | 14.639 |
| 3.5 | 4.255 | 12.254 |
| 4.0 | 3.486 | 10.040 |
| 4.5 | 2.886 | 8.312 |
| 5.0 | 2.380 | 6.854 |
| 5.5 | 1.974 | 5.685 |
| 6.0 | 1.623 | 4.674 |
| 6.5 | 1.403 | 4.041 |
| 7.0 | 1.245 | 3.586 |
| 7.5 | 1.105 | 3.182 |
| 8.0 | 1.003 | 2.889 |
| 8.5 | 908 | 2.615 |
| 9.0 | 817 | 2.353 |
| 9.5 | 717 | 2.065 |
| 10.0 | 615 | 1.771 |
| 10.5 | 520 | 1.498 |

The effective 'K' value is 0.70. 'K' equals effective column length factor. See introduction to column tables showing notation factors

6 X 3 X 3/8 I-BEAM

$A = 4.23 \text{ in}^2$

$r = 0.64 \text{ in}$

$b/t = 8$

| TRUE LENGTH (ft) | F_a (psi) | P_a (lbs) |
|---------------------|----------------|----------------|
| 0.5 | 10.000 | 42.300 |
| 1.0 | 10.000 | 42.300 |
| 1.5 | 10.000 | 42.300 |
| 2.0 | 7.700 | 32.571 |
| 2.5 | 5.415 | 22.905 |
| 3.0 | 4.237 | 17.923 |
| 3.5 | 3.450 | 14.594 |
| 4.0 | 2.833 | 11.984 |
| 4.5 | 2.297 | 9.716 |
| 5.0 | 1.843 | 7.796 |
| 5.5 | 1.563 | 6.611 |
| 6.0 | 1.347 | 5.698 |
| 6.5 | 1.169 | 4.945 |
| 7.0 | 1.050 | 4.442 |
| 7.5 | 923 | 3.904 |
| 8.0 | 800 | 3.384 |
| 8.5 | 721 | 3.050 |
| 9.0 | 647 | 2.737 |
| 9.5 | 586 | 2.479 |
| 10.0 | 525 | 2.221 |
| 10.5 | 479 | 2.026 |

The effective 'K' value is 0.70. 'K' equals effective column length factor. See introduction to column tables showing notation factors

8 X 4 X 3/8 I-BEAM

$A = 5.73 \text{ in}^2$

$r = 0.84 \text{ in}$

$b/t = 10.7$

| TRUE LENGTH (ft) | F_a (psi) | P_a (lbs) |
|---------------------|----------------|----------------|
| 0.5 | 10.000 | 57.300 |
| 1.0 | 10.000 | 57.300 |
| 1.5 | 10.000 | 57.300 |
| 2.0 | 10.000 | 57.300 |
| 2.5 | 8.370 | 47.960 |
| 3.0 | 6.182 | 35.423 |
| 3.5 | 4.917 | 28.174 |
| 4.0 | 4.157 | 23.820 |
| 4.5 | 3.558 | 20.387 |
| 5.0 | 3.063 | 17.551 |
| 5.5 | 2.598 | 14.887 |
| 6.0 | 2.232 | 12.789 |
| 6.5 | 1.888 | 10.818 |
| 7.0 | 1.667 | 9.552 |
| 7.5 | 1.461 | 8.372 |
| 8.0 | 1.311 | 7.512 |
| 8.5 | 1.176 | 6.738 |
| 9.0 | 1.085 | 6.217 |
| 9.5 | 997 | 5.713 |
| 10.0 | 888 | 5.088 |
| 10.5 | 800 | 4.584 |
| 11.0 | 741 | 4.246 |
| 11.5 | 680 | 3.896 |
| 12.0 | 630 | 3.610 |
| 12.5 | 582 | 3.335 |
| 13.0 | 535 | 3.066 |
| 13.5 | 498 | 2.854 |
| 14.0 | 467 | 2.676 |

The effective 'K' value is 0.70. 'K' equals effective column length factor. See introduction to column tables showing notation factors

8 X 4 X 1/2 I-BEAM

$A = 7.51 \text{ in}^2$

$r = 0.85 \text{ in}$

$b/t = 8$

| TRUE LENGTH (ft) | F_a (psi) | P_a (lbs) |
|---------------------|----------------|----------------|
| 0.5 | 10.000 | 75.100 |
| 1.0 | 10.000 | 75.100 |
| 1.5 | 10.000 | 75.100 |
| 2.0 | 10.000 | 75.100 |
| 2.5 | 8.597 | 64.563 |
| 3.0 | 6.303 | 47.336 |
| 3.5 | 5.016 | 37.670 |
| 4.0 | 4.217 | 31.670 |
| 4.5 | 3.620 | 27.186 |
| 5.0 | 3.103 | 23.304 |
| 5.5 | 2.660 | 19.977 |
| 6.0 | 2.282 | 17.138 |
| 6.5 | 1.943 | 14.592 |
| 7.0 | 1.697 | 12.744 |
| 7.5 | 1.485 | 11.152 |
| 8.0 | 1.340 | 10.063 |
| 8.5 | 1.200 | 9.012 |
| 9.0 | 1.102 | 8.276 |
| 9.5 | 1.015 | 7.623 |
| 10.0 | 914 | 6.864 |
| 10.5 | 822 | 6.173 |
| 11.0 | 755 | 5.670 |
| 11.5 | 697 | 5.234 |
| 12.0 | 644 | 4.836 |
| 12.5 | 596 | 4.476 |
| 13.0 | 549 | 4.123 |
| 13.5 | 510 | 3.830 |
| 14.0 | 476 | 3.575 |

The effective 'K' value is 0.70. 'K' equals effective column length factor. See introduction to column tables showing notation factors

10 X 5 X 3/8 I-BEAM

$A = 7.22 \text{ in}^2$

$r = 1.04 \text{ in}$

$b/t = 13.3$

| TRUE LENGTH (ft) | F_a (psi) | P_a (lbs) |
|---------------------|----------------|----------------|
| 0.5 | 8.747 | 63.153 |
| 1.0 | 8.747 | 63.153 |
| 1.5 | 8.747 | 63.153 |
| 2.0 | 8.747 | 63.153 |
| 2.5 | 8.747 | 63.153 |
| 3.0 | 8.747 | 63.153 |
| 3.5 | 6.814 | 49.197 |
| 4.0 | 5.520 | 39.854 |
| 4.5 | 4.711 | 34.013 |
| 5.0 | 4.097 | 29.580 |
| 5.5 | 3.620 | 26.136 |
| 6.0 | 3.186 | 23.003 |
| 6.5 | 2.833 | 20.454 |
| 7.0 | 2.470 | 17.833 |
| 7.5 | 2.188 | 15.797 |
| 8.0 | 1.918 | 13.848 |
| 8.5 | 1.714 | 12.375 |
| 9.0 | 1.540 | 11.119 |
| 9.5 | 1.404 | 10.137 |
| 10.0 | 1.288 | 9.299 |
| 10.5 | 1.179 | 8.512 |
| 11.0 | 1.103 | 7.964 |
| 11.5 | 1.033 | 7.458 |
| 12.0 | 954 | 6.888 |
| 12.5 | 869 | 6.274 |
| 13.0 | 800 | 5.776 |
| 13.5 | 751 | 5.422 |
| 14.0 | 704 | 5.083 |
| 14.5 | 658 | 4.751 |
| 15.0 | 619 | 4.469 |
| 15.5 | 581 | 4.195 |
| 16.0 | 543 | 3.920 |
| 16.5 | 511 | 3.689 |
| 17.0 | 482 | 3.480 |

The effective 'K' value is 0.70. 'K' equals effective column length factor. See introduction to column tables showing notation factors

10 X 5 X 1/2 I-BEAM

$A = 9.51 \text{ in}^2$

$r = 1.05 \text{ in}$

$b/t = 10$

| TRUE LENGTH (ft) | F_a (psi) | P_a (lbs) |
|---------------------|----------------|----------------|
| 0.5 | 10.000 | 95.100 |
| 1.0 | 10.000 | 95.100 |
| 1.5 | 10.000 | 95.100 |
| 2.0 | 10.000 | 95.100 |
| 2.5 | 10.000 | 95.100 |
| 3.0 | 9.163 | 87.140 |
| 3.5 | 6.917 | 65.781 |
| 4.0 | 5.605 | 53.304 |
| 4.5 | 4.765 | 45.315 |
| 5.0 | 4.157 | 39.533 |
| 5.5 | 3.666 | 34.864 |
| 6.0 | 3.227 | 30.689 |
| 6.5 | 2.880 | 27.389 |
| 7.0 | 2.517 | 23.937 |
| 7.5 | 2.232 | 21.226 |
| 8.0 | 1.963 | 18.668 |
| 8.5 | 1.739 | 16.538 |
| 9.0 | 1.564 | 14.874 |
| 9.5 | 1.429 | 13.590 |
| 10.0 | 1.311 | 12.468 |
| 10.5 | 1.200 | 11.412 |
| 11.0 | 1.120 | 10.651 |
| 11.5 | 1.049 | 9.976 |
| 12.0 | 975 | 9.272 |
| 12.5 | 889 | 8.484 |
| 13.0 | 818 | 7.779 |
| 13.5 | 764 | 7.266 |
| 14.0 | 717 | 6.819 |
| 14.5 | 669 | 6.362 |
| 15.0 | 630 | 5.991 |
| 15.5 | 592 | 5.630 |
| 16.0 | 554 | 5.269 |
| 16.5 | 520 | 4.945 |
| 17.0 | 491 | 4.669 |
| 17.5 | 467 | 4.441 |

The effective 'K' value is 0.70. 'K' equals effective column length factor. See introduction to column tables showing notation factors

12 X 6 X 1/2 I-BEAM

A = 11.51 in²

r = 1.26 in

b/t = 12

| TRUE LENGTH (ft) | F _a (psi) | P _a (lbs) |
|---------------------|-------------------------|-------------------------|
| 0.5 | 10.000 | 115.100 |
| 1.0 | 10.000 | 115.100 |
| 1.5 | 10.000 | 115.100 |
| 2.0 | 10.000 | 115.100 |
| 2.5 | 10.000 | 115.100 |
| 3.0 | 10.000 | 115.100 |
| 3.5 | 9.800 | 112.798 |
| 4.0 | 7.502 | 86.348 |
| 4.5 | 6.182 | 71.155 |
| 5.0 | 5.310 | 61.118 |
| 5.5 | 4.653 | 53.556 |
| 6.0 | 4.157 | 47.847 |
| 6.5 | 3.741 | 43.059 |
| 7.0 | 3.364 | 38.720 |
| 7.5 | 3.063 | 35.255 |
| 8.0 | 2.753 | 31.687 |
| 8.5 | 2.458 | 28.292 |
| 9.0 | 2.232 | 25.690 |
| 9.5 | 2.008 | 23.112 |
| 10.0 | 1.793 | 20.637 |
| 10.5 | 1.667 | 19.187 |
| 11.0 | 1.513 | 17.415 |
| 11.5 | 1.411 | 16.241 |
| 12.0 | 1.311 | 15.090 |
| 12.5 | 1.217 | 14.008 |
| 13.0 | 1.144 | 13.167 |
| 13.5 | 1.084 | 12.477 |
| 14.0 | 1.025 | 11.798 |
| 14.5 | 960 | 11.050 |
| 15.0 | 888 | 10.221 |
| 15.5 | 828 | 9.530 |
| 16.0 | 780 | 8.978 |
| 16.5 | 741 | 8.529 |
| 17.0 | 701 | 8.069 |
| 17.5 | 662 | 7.620 |
| 18.0 | 630 | 7.251 |
| 18.5 | 598 | 6.883 |
| 19.0 | 567 | 6.529 |
| 19.5 | 535 | 6.158 |
| 20.0 | 510 | 5.870 |

The effective 'K' value is 0.70. 'K' equals effective column length factor. See introduction to column tables showing notation factors

3 X 3 X 1/4 WIDE-FLANGE BEAM

$$A = 2.13 \text{ in}^2$$

$$r = 0.73 \text{ in}$$

$$b/t = 12$$

| TRUE LENGTH (ft) | F_a (psi) | P_a (lbs) |
|---------------------|----------------|----------------|
| 0.5 | 10.000 | 21.300 |
| 1.0 | 10.000 | 21.300 |
| 1.5 | 10.000 | 21.300 |
| 2.0 | 10.000 | 21.300 |
| 2.5 | 7.271 | 15.487 |
| 3.0 | 5.915 | 12.599 |
| 3.5 | 5.046 | 10.748 |
| 4.0 | 4.318 | 9.197 |
| 4.5 | 3.667 | 7.811 |
| 5.0 | 3.105 | 6.614 |
| 5.5 | 2.647 | 5.638 |
| 6.0 | 2.208 | 4.703 |
| 6.5 | 1.907 | 4.062 |
| 7.0 | 1.597 | 3.402 |
| 7.5 | 1.412 | 3.008 |
| 8.0 | 1.274 | 3.714 |
| 8.5 | 1.145 | 2.439 |
| 9.0 | 1.048 | 2.232 |
| 9.5 | 965 | 2.055 |
| 10.0 | 883 | 1.881 |
| 10.5 | 803 | 1.710 |
| 11.0 | 719 | 1.531 |
| 11.5 | 633 | 1.348 |
| 12.0 | 547 | 1.165 |

The effective 'K' value is 0.70. 'K' equals effective column length factor. See introduction to column tables showing notation factors

4 X 4 X 1/4 WIDE-FLANGE BEAM

$A = 2.89 \text{ in}^2$

$r = 0.96 \text{ in}$

$b/t = 16$

| TRUE LENGTH (ft) | F_a (psi) | P_a (lbs) |
|---------------------|----------------|----------------|
| 0.5 | 7,208 | 20,831 |
| 1.0 | 7,208 | 20,831 |
| 1.5 | 7,208 | 20,831 |
| 2.0 | 7,208 | 20,831 |
| 2.5 | 7,208 | 20,831 |
| 3.0 | 7,208 | 20,831 |
| 3.5 | 6,697 | 19,354 |
| 4.0 | 5,838 | 16,872 |
| 4.5 | 5,155 | 14,898 |
| 5.0 | 4,621 | 13,355 |
| 5.5 | 4,050 | 11,705 |
| 6.0 | 3,583 | 10,355 |
| 6.5 | 3,163 | 9,141 |
| 7.0 | 2,792 | 8,069 |
| 7.5 | 2,452 | 7,115 |
| 8.0 | 2,150 | 6,214 |
| 8.5 | 1,923 | 5,557 |
| 9.0 | 1,683 | 4,864 |
| 9.5 | 1,503 | 4,344 |
| 10.0 | 1,383 | 3,997 |
| 10.5 | 1,278 | 3,693 |
| 11.0 | 1,174 | 3,393 |
| 11.5 | 1,095 | 3,165 |
| 12.0 | 1,027 | 2,968 |
| 12.5 | 964 | 2,786 |
| 13.0 | 902 | 2,607 |
| 13.5 | 843 | 2,436 |
| 14.0 | 777 | 2,246 |
| 14.5 | 714 | 2,063 |
| 15.0 | 652 | 1,884 |
| 15.5 | 582 | 1,682 |
| 16.0 | 520 | 1,503 |

The effective 'K' value is 0.70. 'K' equals effective column length factor. See introduction to column tables showing notation factors

6 X 6 X 1/4 WIDE-FLANGE BEAM

A = 4.39 in²

r = 1.43 in

b/t = 24

| TRUE LENGTH (ft) | F _a (psi) | P _a (lbs) |
|------------------|----------------------|----------------------|
| 0.5 | 4.167 | 18.293 |
| 1.0 | 4.167 | 18.293 |
| 1.5 | 4.167 | 18.293 |
| 2.0 | 4.167 | 18.293 |
| 2.5 | 4.167 | 18.293 |
| 3.0 | 4.167 | 18.293 |
| 3.5 | 4.167 | 18.293 |
| 4.0 | 4.167 | 18.293 |
| 4.5 | 4.167 | 18.293 |
| 5.0 | 4.167 | 18.293 |
| 5.5 | 4.167 | 18.293 |
| 6.0 | 4.167 | 18.293 |
| 6.5 | 4.167 | 18.293 |
| 7.0 | 3.997 | 17.547 |
| 7.5 | 3.666 | 16.094 |
| 8.0 | 3.334 | 14.636 |
| 8.5 | 3.068 | 13.469 |
| 9.0 | 2.800 | 12.292 |
| 9.5 | 2.534 | 11.124 |
| 10.0 | 2.322 | 10.194 |
| 10.5 | 2.097 | 9.206 |
| 11.0 | 1.917 | 8.416 |
| 11.5 | 1.754 | 7.700 |
| 12.0 | 1.644 | 7.217 |
| 12.5 | 1.510 | 6.629 |
| 13.0 | 1.419 | 6.229 |
| 13.5 | 1.332 | 5.847 |
| 14.0 | 1.244 | 5.461 |
| 14.5 | 1.171 | 5.141 |
| 15.0 | 1.118 | 4.908 |
| 15.5 | 1.066 | 4.680 |
| 16.0 | 1.013 | 4.447 |
| 16.5 | 954 | 4.188 |
| 17.0 | 891 | 3.911 |
| 17.5 | 834 | 3.661 |
| 18.0 | 792 | 3.477 |
| 18.5 | 756 | 3.319 |
| 19.0 | 722 | 3.170 |
| 19.5 | 687 | 3.016 |
| 20.0 | 655 | 2.875 |

The effective 'K' value is 0.70. 'K' equals effective column length factor. See introduction to column tables showing notation factors

6 X 6 X 3/8 WIDE-FLANGE BEAM

A = 6.48 in²

r = 1.44 in

b/t = 16

| TRUE LENGTH (ft) | F _a (psi) | P _a (lbs) |
|---------------------|-------------------------|-------------------------|
| 0.5 | 6.233 | 40.390 |
| 1.0 | 6.233 | 40.390 |
| 1.5 | 6.233 | 40.390 |
| 2.0 | 6.233 | 40.390 |
| 2.5 | 6.233 | 40.390 |
| 3.0 | 6.233 | 40.390 |
| 3.5 | 6.233 | 40.390 |
| 4.0 | 6.233 | 40.390 |
| 4.5 | 6.233 | 40.390 |
| 5.0 | 6.233 | 40.390 |
| 5.5 | 5.586 | 36.197 |
| 6.0 | 4.917 | 31.862 |
| 6.5 | 4.447 | 28.817 |
| 7.0 | 4.037 | 26.160 |
| 7.5 | 3.695 | 23.944 |
| 8.0 | 3.365 | 21.805 |
| 8.5 | 3.093 | 20.043 |
| 9.0 | 2.833 | 18.358 |
| 9.5 | 2.563 | 16.608 |
| 10.0 | 2.345 | 15.196 |
| 10.5 | 2.123 | 13.757 |
| 11.0 | 1.948 | 12.623 |
| 11.5 | 1.774 | 11.496 |
| 12.0 | 1.667 | 10.802 |
| 12.5 | 1.528 | 9.901 |
| 13.0 | 1.436 | 9.305 |
| 13.5 | 1.347 | 8.729 |
| 14.0 | 1.260 | 8.165 |
| 14.5 | 1.206 | 7.815 |
| 15.0 | 1.129 | 7.316 |
| 15.5 | 1.076 | 6.972 |
| 16.0 | 1.025 | 6.642 |
| 16.5 | 969 | 6.279 |
| 17.0 | 906 | 5.871 |
| 17.5 | 845 | 5.476 |
| 18.0 | 800 | 5.184 |
| 18.5 | 765 | 4.957 |
| 19.0 | 731 | 4.737 |
| 19.5 | 696 | 4.510 |
| 20.0 | 662 | 4.290 |

The effective 'K' value is 0.70. 'K' equals effective column length factor. See introduction to column tables showing notation factors

8 X 8 X 3/8 WIDE-FLANGE BEAM

A = 8.73 in²

r = 1.92 in

b/t = 21.3

| TRUE LENGTH (ft) | F _a (psi) | P _a (lbs) |
|---------------------|-------------------------|-------------------------|
| 0.5 | 4.483 | 39.137 |
| 1.0 | 4.483 | 39.137 |
| 1.5 | 4.483 | 39.137 |
| 2.0 | 4.483 | 39.137 |
| 2.5 | 4.483 | 39.137 |
| 3.0 | 4.483 | 39.137 |
| 3.5 | 4.483 | 39.137 |
| 4.0 | 4.483 | 39.137 |
| 4.5 | 4.483 | 39.137 |
| 5.0 | 4.483 | 39.137 |
| 5.5 | 4.483 | 39.137 |
| 6.0 | 4.483 | 39.137 |
| 6.5 | 4.483 | 39.137 |
| 7.0 | 4.483 | 39.137 |
| 7.5 | 4.483 | 39.137 |
| 8.0 | 4.483 | 39.137 |
| 8.5 | 4.483 | 39.137 |
| 9.0 | 4.237 | 36.989 |
| 9.5 | 3.927 | 34.283 |
| 10.0 | 3.695 | 32.257 |
| 10.5 | 3.450 | 30.119 |
| 11.0 | 3.213 | 28.049 |
| 11.5 | 3.038 | 26.522 |
| 12.0 | 2.833 | 24.732 |
| 12.5 | 2.627 | 22.934 |
| 13.0 | 2.442 | 21.319 |
| 13.5 | 2.297 | 20.053 |
| 14.0 | 2.129 | 18.586 |
| 14.5 | 2.003 | 17.486 |
| 15.0 | 1.843 | 16.089 |
| 15.5 | 1.744 | 15.225 |
| 16.0 | 1.667 | 14.553 |
| 16.5 | 1.563 | 13.645 |
| 17.0 | 1.477 | 12.894 |
| 17.5 | 1.413 | 12.335 |
| 18.0 | 1.348 | 11.768 |
| 18.5 | 1.283 | 11.201 |
| 19.0 | 1.220 | 10.651 |
| 19.5 | 1.169 | 10.205 |
| 20.0 | 1.129 | 9.856 |

The effective 'K' value is 0.70. 'K' equals effective column length factor. See introduction to column tables showing notation factors

8 X 8 X 1/2 WIDE-FLANGE BEAM

$A = 11.51 \text{ in}^2$

$r = 1.93 \text{ in}$

$b/t = 16$

| TRUE LENGTH (ft) | F_a (psi) | P_a (lbs) |
|---------------------|----------------|----------------|
| 0.5 | 6.233 | 71.742 |
| 1.0 | 6.233 | 71.742 |
| 1.5 | 6.233 | 71.742 |
| 2.0 | 6.233 | 71.742 |
| 2.5 | 6.233 | 71.742 |
| 3.0 | 6.233 | 71.742 |
| 3.5 | 6.233 | 71.742 |
| 4.0 | 6.233 | 71.742 |
| 4.5 | 6.233 | 71.742 |
| 5.0 | 6.233 | 71.742 |
| 5.5 | 6.233 | 71.742 |
| 6.0 | 6.233 | 71.742 |
| 6.5 | 6.233 | 71.742 |
| 7.0 | 6.037 | 69.486 |
| 7.5 | 5.460 | 62.845 |
| 8.0 | 4.966 | 57.159 |
| 8.5 | 4.606 | 53.015 |
| 9.0 | 4.267 | 49.133 |
| 9.5 | 3.957 | 45.545 |
| 10.0 | 3.718 | 42.794 |
| 10.5 | 3.475 | 39.997 |
| 11.0 | 3.240 | 37.292 |
| 11.5 | 3.058 | 35.198 |
| 12.0 | 2.860 | 32.919 |
| 12.5 | 2.653 | 30.536 |
| 13.0 | 2.470 | 28.430 |
| 13.5 | 2.321 | 26.715 |
| 14.0 | 2.158 | 24.839 |
| 14.5 | 2.023 | 23.285 |
| 15.0 | 1.868 | 21.501 |
| 15.5 | 1.757 | 20.223 |
| 16.0 | 1.679 | 19.325 |
| 16.5 | 1.580 | 18.186 |
| 17.0 | 1.491 | 17.161 |
| 17.5 | 1.425 | 16.402 |
| 18.0 | 1.360 | 15.654 |
| 18.5 | 1.296 | 14.917 |
| 19.0 | 1.231 | 14.169 |
| 19.5 | 1.179 | 13.570 |
| 20.0 | 1.137 | 13.087 |

The effective 'K' value is 0.70. 'K' equals effective column length factor. See introduction to column tables showing notation factors

10 X 10 X 3/8 WIDE-FLANGE BEAM

$A = 11.06 \text{ in}^2$

$r = 2.38 \text{ in}$

$b/t = 26.7$

| TRUE LENGTH (ft) | F_a (psi) | P_a (lbs) |
|------------------|-------------|-------------|
| 0.5 | 2.732 | 30.216 |
| 1.0 | 2.732 | 30.216 |
| 1.5 | 2.732 | 30.216 |
| 2.0 | 2.732 | 30.216 |
| 2.5 | 2.732 | 30.216 |
| 3.0 | 2.732 | 30.216 |
| 3.5 | 2.732 | 30.216 |
| 4.0 | 2.732 | 30.216 |
| 4.5 | 2.732 | 30.216 |
| 5.0 | 2.732 | 30.216 |
| 5.5 | 2.732 | 30.216 |
| 6.0 | 2.732 | 30.216 |
| 6.5 | 2.732 | 30.216 |
| 7.0 | 2.732 | 30.216 |
| 7.5 | 2.732 | 30.216 |
| 8.0 | 2.732 | 30.216 |
| 8.5 | 2.732 | 30.216 |
| 9.0 | 2.732 | 30.216 |
| 9.5 | 2.732 | 30.216 |
| 10.0 | 2.732 | 30.216 |
| 10.5 | 2.732 | 30.216 |
| 11.0 | 2.732 | 30.216 |
| 11.5 | 2.732 | 30.216 |
| 12.0 | 2.732 | 30.216 |
| 12.5 | 2.732 | 30.216 |
| 13.0 | 2.732 | 30.216 |
| 13.5 | 2.732 | 30.216 |
| 14.0 | 2.732 | 30.216 |
| 14.5 | 2.732 | 30.216 |
| 15.0 | 2.732 | 30.216 |
| 15.5 | 2.621 | 28.988 |
| 16.0 | 2.476 | 27.385 |
| 16.5 | 2.349 | 25.980 |
| 17.0 | 2.232 | 24.686 |
| 17.5 | 2.093 | 23.149 |
| 18.0 | 1.993 | 22.043 |
| 18.5 | 1.868 | 20.660 |
| 19.0 | 1.773 | 19.609 |
| 19.5 | 1.709 | 18.902 |
| 20.0 | 1.640 | 18.138 |

The effective 'K' value is 0.70. 'K' equals effective column length factor. See introduction to column tables showing notation factors

10 X 10 X 1/2 WIDE-FLANGE BEAM

$A = 14.51 \text{ in}^2$

$r = 2.4 \text{ in}$

$b/t = 20$

| TRUE LENGTH (ft) | F_a (psi) | P_a (lbs) |
|------------------|-------------|-------------|
| 0.5 | 4.920 | 71.389 |
| 1.0 | 4.920 | 71.389 |
| 1.5 | 4.920 | 71.389 |
| 2.0 | 4.920 | 71.389 |
| 2.5 | 4.920 | 71.389 |
| 3.0 | 4.920 | 71.389 |
| 3.5 | 4.920 | 71.389 |
| 4.0 | 4.920 | 71.389 |
| 4.5 | 4.920 | 71.389 |
| 5.0 | 4.920 | 71.389 |
| 5.5 | 4.920 | 71.389 |
| 6.0 | 4.920 | 71.389 |
| 6.5 | 4.920 | 71.389 |
| 7.0 | 4.920 | 71.389 |
| 7.5 | 4.920 | 71.389 |
| 8.0 | 4.920 | 71.389 |
| 8.5 | 4.920 | 71.389 |
| 9.0 | 4.920 | 71.389 |
| 9.5 | 4.920 | 71.389 |
| 10.0 | 4.917 | 71.346 |
| 10.5 | 4.641 | 67.341 |
| 11.0 | 4.367 | 63.365 |
| 11.5 | 4.117 | 59.738 |
| 12.0 | 3.867 | 56.110 |
| 12.5 | 3.695 | 53.614 |
| 13.0 | 3.500 | 50.785 |
| 13.5 | 3.304 | 47.941 |
| 14.0 | 3.133 | 45.460 |
| 14.5 | 2.999 | 43.515 |
| 15.0 | 2.833 | 41.107 |
| 15.5 | 2.966 | 43.037 |
| 16.0 | 2.517 | 36.522 |
| 16.5 | 2.379 | 34.519 |
| 17.0 | 2.267 | 32.894 |
| 17.5 | 2.129 | 30.892 |
| 18.0 | 2.033 | 29.499 |
| 18.5 | 1.908 | 27.685 |
| 19.0 | 1.800 | 26.118 |
| 19.5 | 1.729 | 25.088 |
| 20.0 | 1.667 | 24.188 |

The effective 'K' value is 0.70. 'K' equals effective column length factor. See introduction to column tables showing notation factors

12 X 12 X 1/2 WIDE-FLANGE BEAM

A = 17.51 in²
r = 2.87 in
b/t = 24

| TRUE LENGTH (ft) | F _a (psi) | P _a (lbs) |
|------------------|----------------------|----------------------|
| 0.5 | 3.608 | 63.176 |
| 1.0 | 3.608 | 63.176 |
| 1.5 | 3.608 | 63.176 |
| 2.0 | 3.608 | 63.176 |
| 2.5 | 3.608 | 63.176 |
| 3.0 | 3.608 | 63.176 |
| 3.5 | 3.608 | 63.176 |
| 4.0 | 3.608 | 63.176 |
| 4.5 | 3.608 | 63.176 |
| 5.0 | 3.608 | 63.176 |
| 5.5 | 3.608 | 63.176 |
| 6.0 | 3.608 | 63.176 |
| 6.5 | 3.608 | 63.176 |
| 7.0 | 3.608 | 63.176 |
| 7.5 | 3.608 | 63.176 |
| 8.0 | 3.608 | 63.176 |
| 8.5 | 3.608 | 63.176 |
| 9.0 | 3.608 | 63.176 |
| 9.5 | 3.608 | 63.176 |
| 10.0 | 3.608 | 63.176 |
| 10.5 | 3.608 | 63.176 |
| 11.0 | 3.608 | 63.176 |
| 11.5 | 3.608 | 63.176 |
| 12.0 | 3.608 | 63.176 |
| 12.5 | 3.608 | 63.176 |
| 13.0 | 3.608 | 63.176 |
| 13.5 | 3.608 | 63.176 |
| 14.0 | 3.608 | 63.176 |
| 14.5 | 3.608 | 63.176 |
| 15.0 | 3.608 | 63.176 |
| 15.5 | 3.516 | 61.565 |
| 16.0 | 3.349 | 58.641 |
| 16.5 | 3.200 | 56.032 |
| 17.0 | 3.078 | 53.896 |
| 17.5 | 2.954 | 51.725 |
| 18.0 | 2.813 | 49.256 |
| 18.5 | 2.673 | 46.804 |
| 19.0 | 2.552 | 44.686 |
| 19.5 | 2.429 | 42.532 |
| 20.0 | 2.333 | 40.851 |

The effective 'K' value is 0.70. 'K' equals effective column length factor. See introduction to column tables showing notation factors

2 X 2 X 1/4 SQUARE TUBE

$A = 1.74 \text{ in}^2$

$r = 0.73 \text{ in}$

$b/t = 8$

| TRUE LENGTH (ft) | F_a (psi) | P_a (lbs) |
|---------------------|----------------|----------------|
| 0.5 | 10.000 | 17.400 |
| 1.0 | 10.000 | 17.400 |
| 1.5 | 10.000 | 17.400 |
| 2.0 | 9.850 | 17.139 |
| 2.5 | 8.650 | 15.051 |
| 3.0 | 7.450 | 12.963 |
| 3.5 | 6.491 | 11.294 |
| 4.0 | 5.684 | 9.890 |
| 4.5 | 5.000 | 8.700 |
| 5.0 | 4.253 | 7.400 |
| 5.5 | 3.726 | 6.483 |
| 6.0 | 3.188 | 5.547 |
| 6.5 | 2.786 | 4.848 |
| 7.0 | 2.454 | 4.270 |
| 7.5 | 2.111 | 3.673 |
| 8.0 | 1.895 | 3.297 |
| 8.5 | 1.722 | 2.996 |
| 9.0 | 1.585 | 2.758 |
| 9.5 | 1.448 | 2.520 |
| 10.0 | 1.370 | 2.384 |
| 10.5 | 1.276 | 2.220 |
| 11.0 | 1.189 | 2.069 |
| 11.5 | 1.079 | 1.877 |
| 12.0 | 957 | 1.665 |

The effective 'K' value is 0.70. 'K' equals effective column length factor. See introduction to column tables showing notation factors

2-1/2 X 2-1/2 X 1/4 SQUARE TUBE

$A = 2.24 \text{ in}^2$

$r = 0.92 \text{ in}$

$b/t = 10$

| TRUE LENGTH (ft) | F_a (psi) | P_a (lbs) |
|---------------------|----------------|----------------|
| 0.5 | 10.000 | 22.400 |
| 1.0 | 10.000 | 22.400 |
| 1.5 | 10.000 | 22.400 |
| 2.0 | 10.000 | 22.400 |
| 2.5 | 9.900 | 22.176 |
| 3.0 | 8.816 | 19.748 |
| 3.5 | 7.842 | 17.566 |
| 4.0 | 7.078 | 15.855 |
| 4.5 | 6.351 | 14.226 |
| 5.0 | 5.733 | 12.842 |
| 5.5 | 5.192 | 11.630 |
| 6.0 | 4.675 | 10.472 |
| 6.5 | 4.146 | 9.287 |
| 7.0 | 3.673 | 8.228 |
| 7.5 | 3.246 | 7.271 |
| 8.0 | 2.904 | 6.505 |
| 8.5 | 2.629 | 5.889 |
| 9.0 | 2.358 | 5.282 |
| 9.5 | 2.087 | 4.675 |
| 10.0 | 1.923 | 4.308 |
| 10.5 | 1.825 | 4.088 |
| 11.0 | 1.641 | 3.676 |
| 11.5 | 1.533 | 3.434 |
| 12.0 | 1.445 | 3.237 |
| 12.5 | 1.387 | 3.107 |
| 13.0 | 1.320 | 2.957 |
| 13.5 | 1.239 | 2.775 |
| 14.0 | 1.163 | 2.605 |
| 14.5 | 1.077 | 2.412 |
| 15.0 | 977 | 2.188 |

The effective 'K' value is 0.70. 'K' equals effective column length factor. See introduction to column tables showing notation factors

3 X 3 X 1/4 SQUARE TUBE

$A = 2.74 \text{ in}^2$

$r = 1.13 \text{ in}$

$b/t = 12$

| TRUE LENGTH (ft) | F_a (psi) | P_a (lbs) |
|------------------|-------------|-------------|
| 0.5 | 8.880 | 24.331 |
| 1.0 | 8.880 | 24.331 |
| 1.5 | 8.880 | 24.331 |
| 2.0 | 8.880 | 24.331 |
| 2.5 | 8.880 | 24.331 |
| 3.0 | 8.880 | 24.331 |
| 3.5 | 8.880 | 24.331 |
| 4.0 | 8.273 | 22.668 |
| 4.5 | 7.573 | 20.750 |
| 5.0 | 6.976 | 19.114 |
| 5.5 | 6.386 | 17.498 |
| 6.0 | 5.857 | 16.048 |
| 6.5 | 5.416 | 14.840 |
| 7.0 | 4.977 | 13.637 |
| 7.5 | 4.566 | 12.511 |
| 8.0 | 4.133 | 11.324 |
| 8.5 | 3.732 | 10.226 |
| 9.0 | 3.397 | 9.308 |
| 9.5 | 3.046 | 8.346 |
| 10.0 | 2.821 | 7.730 |
| 10.5 | 2.604 | 7.135 |
| 11.0 | 2.383 | 6.529 |
| 11.5 | 2.163 | 5.927 |
| 12.0 | 2.013 | 5.516 |
| 12.5 | 1.865 | 5.110 |
| 13.0 | 1.748 | 4.790 |
| 13.5 | 1.643 | 4.502 |
| 14.0 | 1.565 | 4.288 |
| 14.5 | 1.467 | 4.020 |
| 15.0 | 1.428 | 3.913 |
| 15.5 | 1.367 | 3.746 |
| 16.0 | 1.308 | 3.584 |
| 16.5 | 1.248 | 3.420 |
| 17.0 | 1.193 | 3.269 |
| 17.5 | 1.121 | 3.072 |
| 18.0 | 1.052 | 2.882 |

The effective 'K' value is 0.70. 'K' equals effective column length factor. See introduction to column tables showing

4 X 4 X 1/4 SQUARE TUBE

A = 3.74 in²

r = 1.53 in

b/t = 16

| TRUE LENGTH (ft) | F _a (psi) | P _a (lbs) |
|---------------------|-------------------------|-------------------------|
| 0.5 | 6.595 | 24.665 |
| 1.0 | 6.595 | 24.665 |
| 1.5 | 6.595 | 24.665 |
| 2.0 | 6.595 | 24.665 |
| 2.5 | 6.595 | 24.665 |
| 3.0 | 6.595 | 24.665 |
| 3.5 | 6.595 | 24.665 |
| 4.0 | 6.595 | 24.665 |
| 4.5 | 6.595 | 24.665 |
| 5.0 | 6.595 | 24.665 |
| 5.5 | 6.595 | 24.665 |
| 6.0 | 6.595 | 24.665 |
| 6.5 | 6.595 | 24.665 |
| 7.0 | 6.595 | 24.665 |
| 7.5 | 6.349 | 23.745 |
| 8.0 | 5.941 | 22.219 |
| 8.5 | 5.608 | 20.974 |
| 9.0 | 5.283 | 19.758 |
| 9.5 | 4.962 | 18.558 |
| 10.0 | 4.666 | 17.451 |
| 10.5 | 4.306 | 16.104 |
| 11.0 | 4.025 | 15.054 |
| 11.5 | 3.738 | 13.980 |
| 12.0 | 3.493 | 13.064 |
| 12.5 | 3.233 | 12.091 |
| 13.0 | 3.000 | 11.220 |
| 13.5 | 2.836 | 10.607 |
| 14.0 | 2.672 | 9.993 |
| 14.5 | 2.511 | 9.391 |
| 15.0 | 2.350 | 8.789 |
| 15.5 | 2.225 | 8.322 |
| 16.0 | 2.052 | 7.674 |
| 16.5 | 1.948 | 7.286 |
| 17.0 | 1.850 | 6.919 |
| 17.5 | 1.767 | 6.609 |
| 18.0 | 1.687 | 6.309 |
| 18.5 | 1.631 | 6.100 |
| 19.0 | 1.558 | 5.827 |
| 19.5 | 1.484 | 5.550 |
| 20.0 | 1.441 | 5.389 |

The effective 'K' value is 0.70. 'K' equals effective column length factor. See introduction to column tables showing notation factors